

GaN/SiC Transistors— Fight or Flight?

Getting EMC ready for the next generation of power electronics devices



About Us

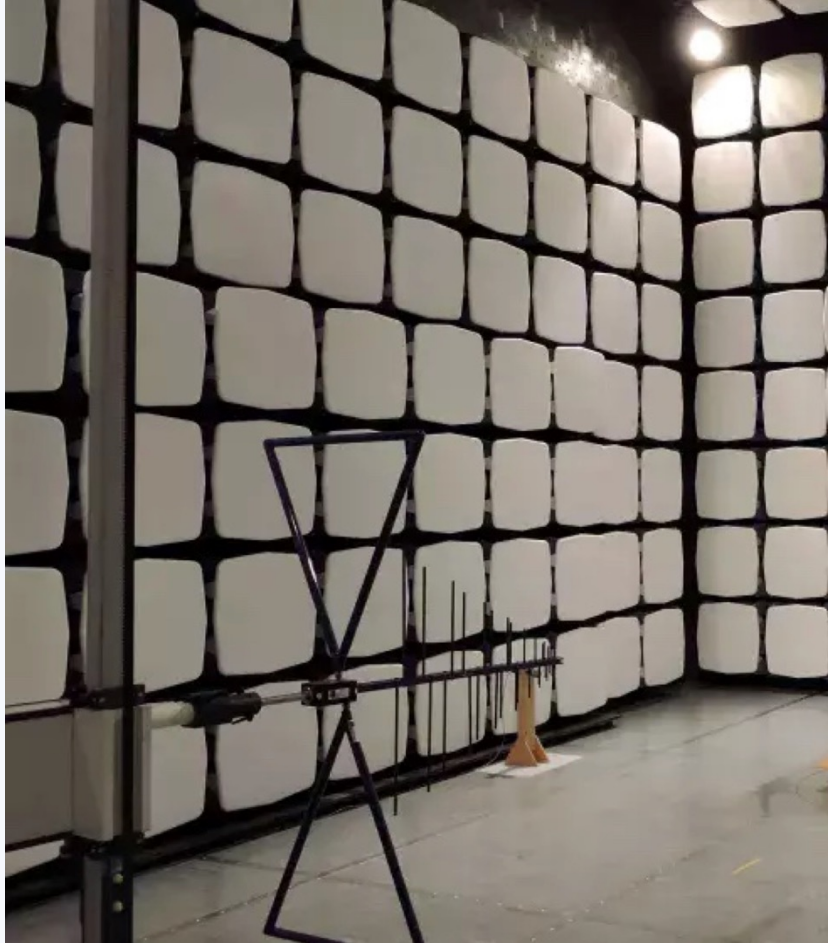


Dr. Yegi Bonyadi currently works as Electronics Team Leader at Lyra Electronics Ltd (<https://www.lyraelectronics.com>), where she focuses on the design of automotive high-power DC-DC converters, on-board chargers and cost-effective EMC design. Her interests include power converter design, automotive power inverters, Hybrid/electric vehicles, power electronics modelling, and Wide-Bandgap semiconductor power devices.



Dr. Min Zhang is the founder and principal EMC consultant of Mach One Design Ltd (www.mach1design.co.uk), a UK-based engineering firm that specializes in EMC consulting, troubleshooting, and training. His in-depth knowledge of power electronics, digital electronics, electric machines, and product design has benefitted companies worldwide. Zhang can be reached at info@mach1design.co.uk

Outline of the Workshop



- EMI Challenges Unveiled
- Demystifying EMC Part 1: Finding Your “Ground”
- Demystifying EMC Part 2: Parastics & Coupling
- Effective EMC Testing Part 1: The Benchttop Approach
- Effective EMC Testing Part 2: The Chamber Approach
- Design Strategies for Achieving EMC Compliance
- A case study
- Q & A Session

GaN & SiC Transistors – Typical Applications



GaN Charger 108W, Belkin, Source: Apple.com

- Mobile phone/Laptop chargers
- Home appliance motor drive applications
- Wireless charging for phones/laptops
- LIDARs
- RF Amplifiers



Lyra's 22kW SiC Bi-directional On-board Charger

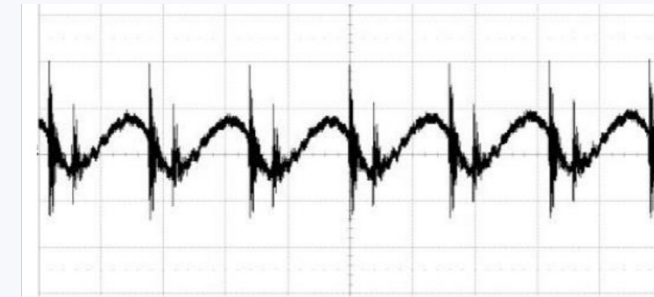
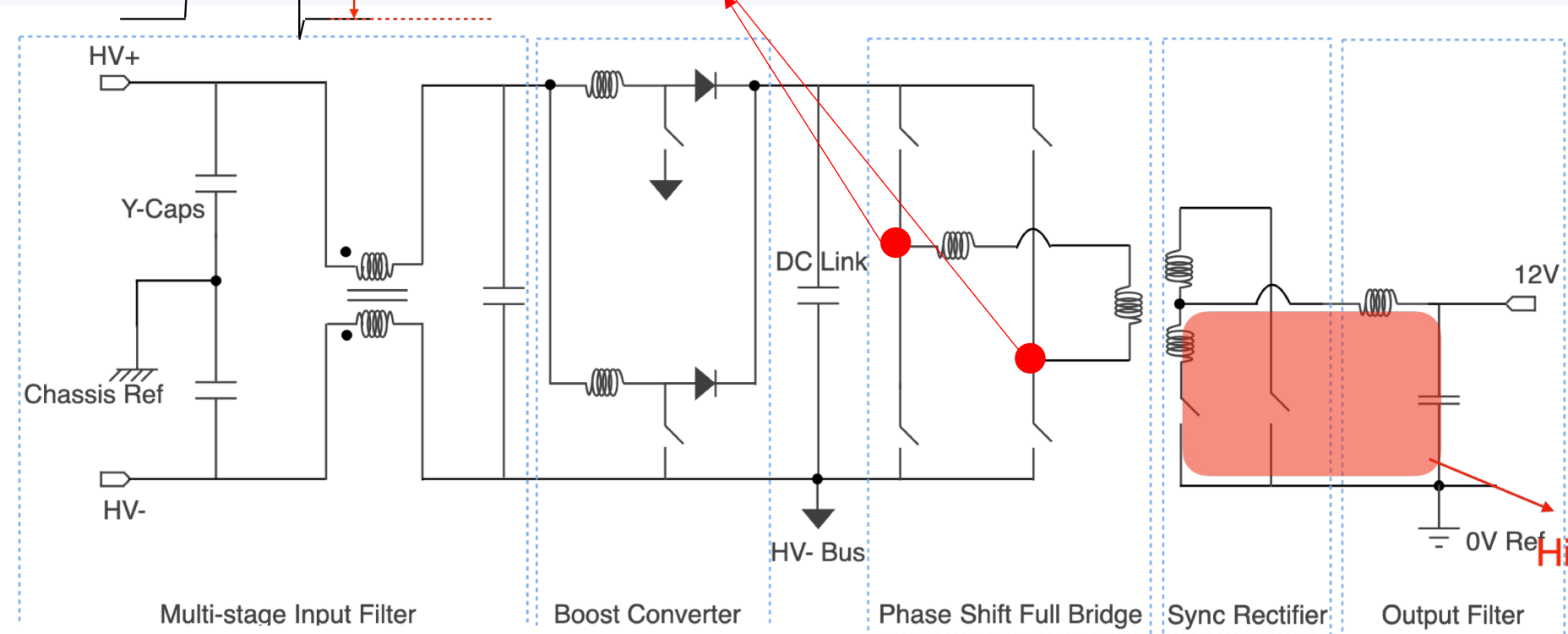
- Industrial/EV motor drive applications
- Solar inverters
- High power & high-temperature applications
- RF and microwave applications (typically, Military applications)

New Challenges

Overshoot voltage depends on the design

V_{BAT} , typically 400V-800V

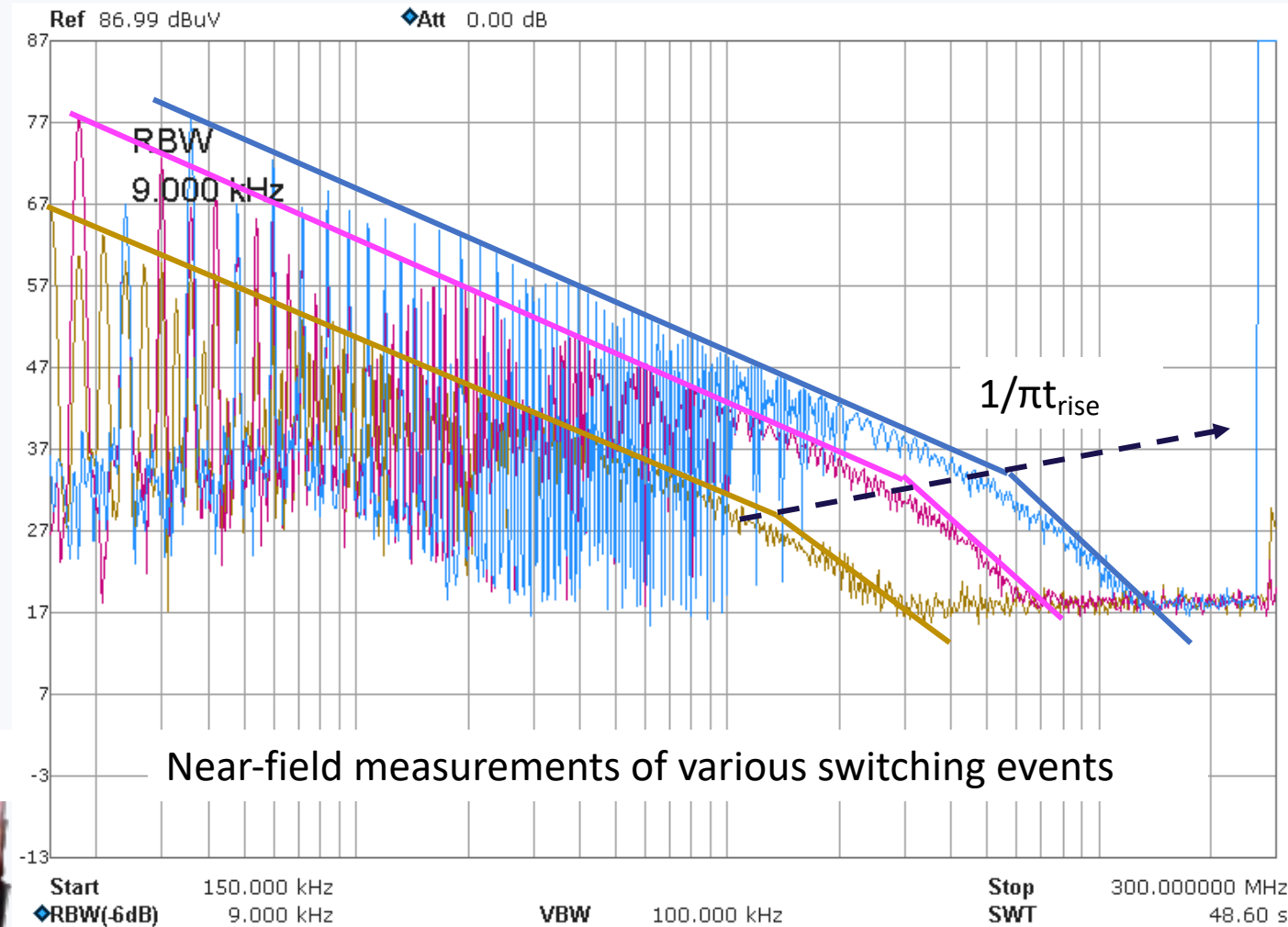
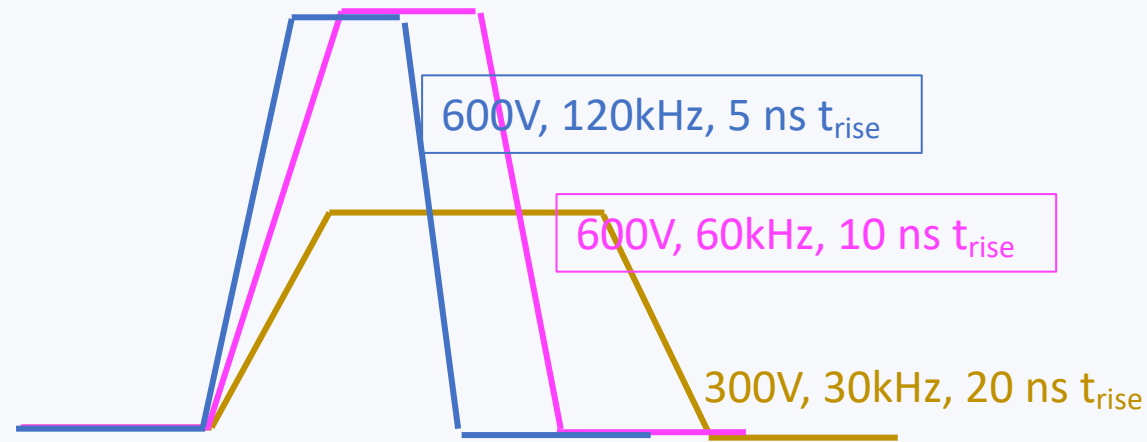
- High dV/dt noise, for example, motor drives, DC-DCs, and On-board-chargers
- High di/dt noise loop, e.g. motor drives, DC-DCs
- Galvanic isolation provides a safety feature, but the transformer cannot block high-frequency radio frequency (RF) signals



High di/dt current loop

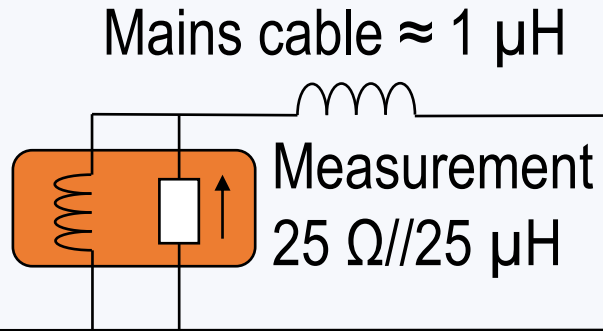
Simplified Schematics of a DC-DC Converter

Need for Speed?

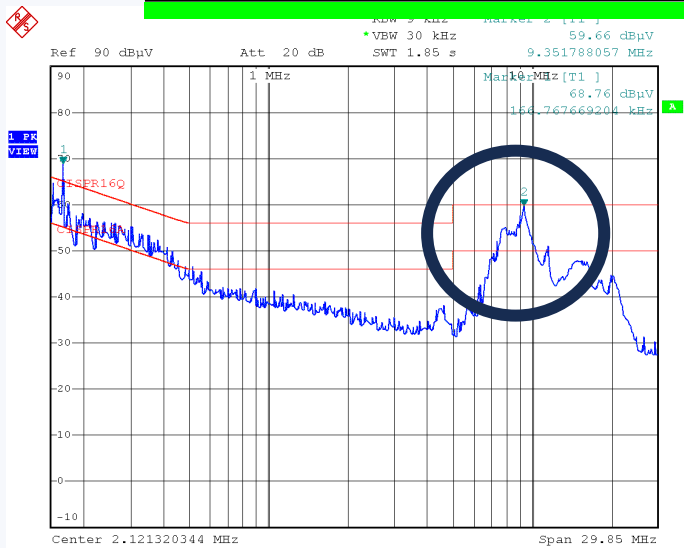
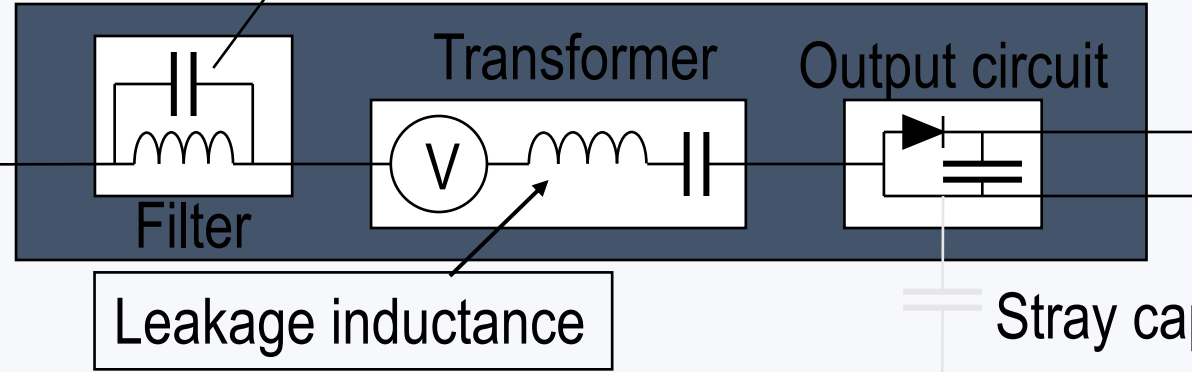


Conducted Emissions - The 10-30 MHz "Hump"

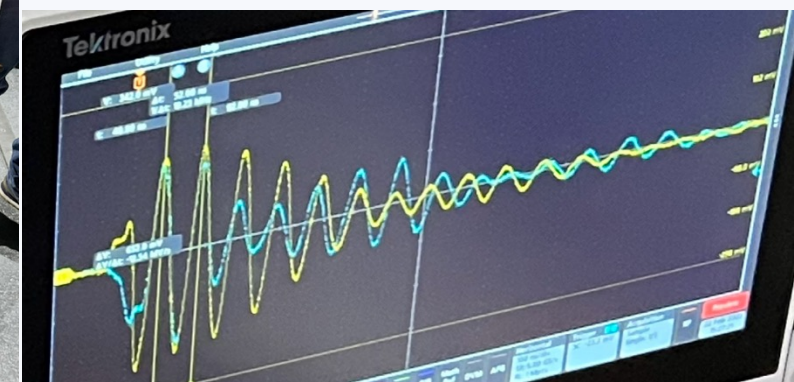
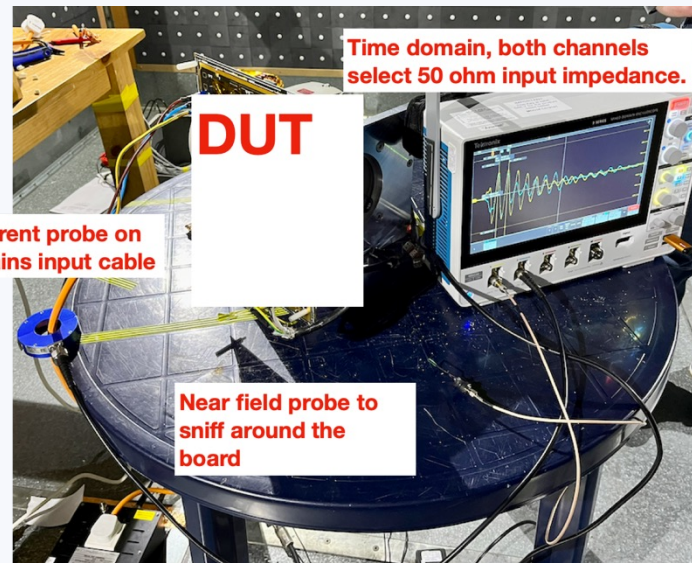
Common mode equivalent circuit



Choke self capacitance

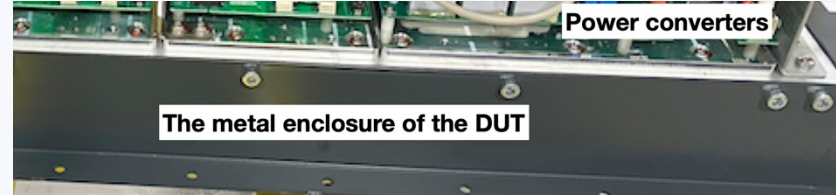
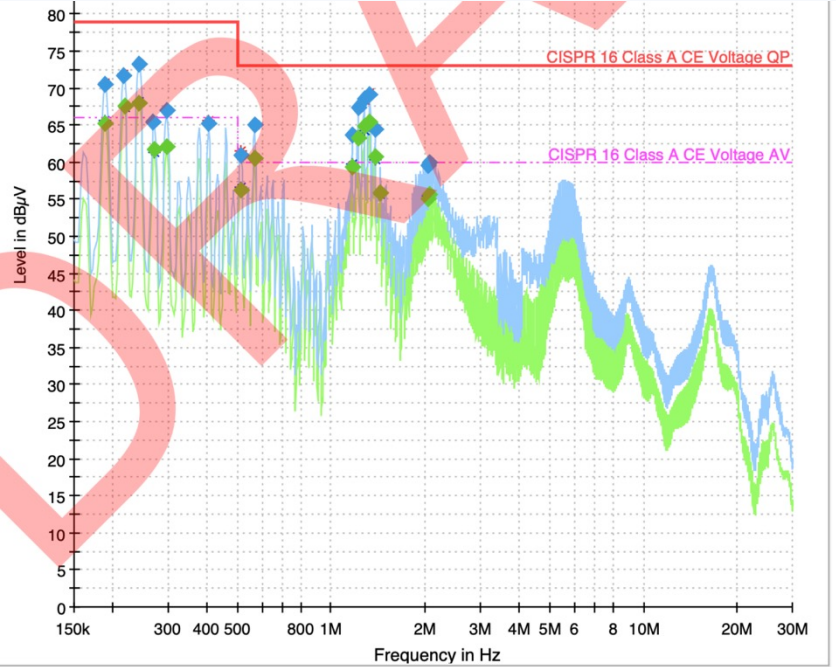


Resonance

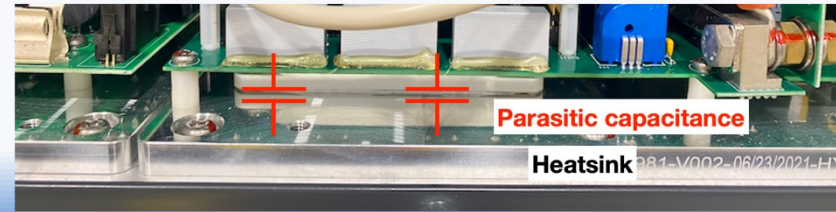


Conducted Emission Test Result of a SiC PFC Circuit

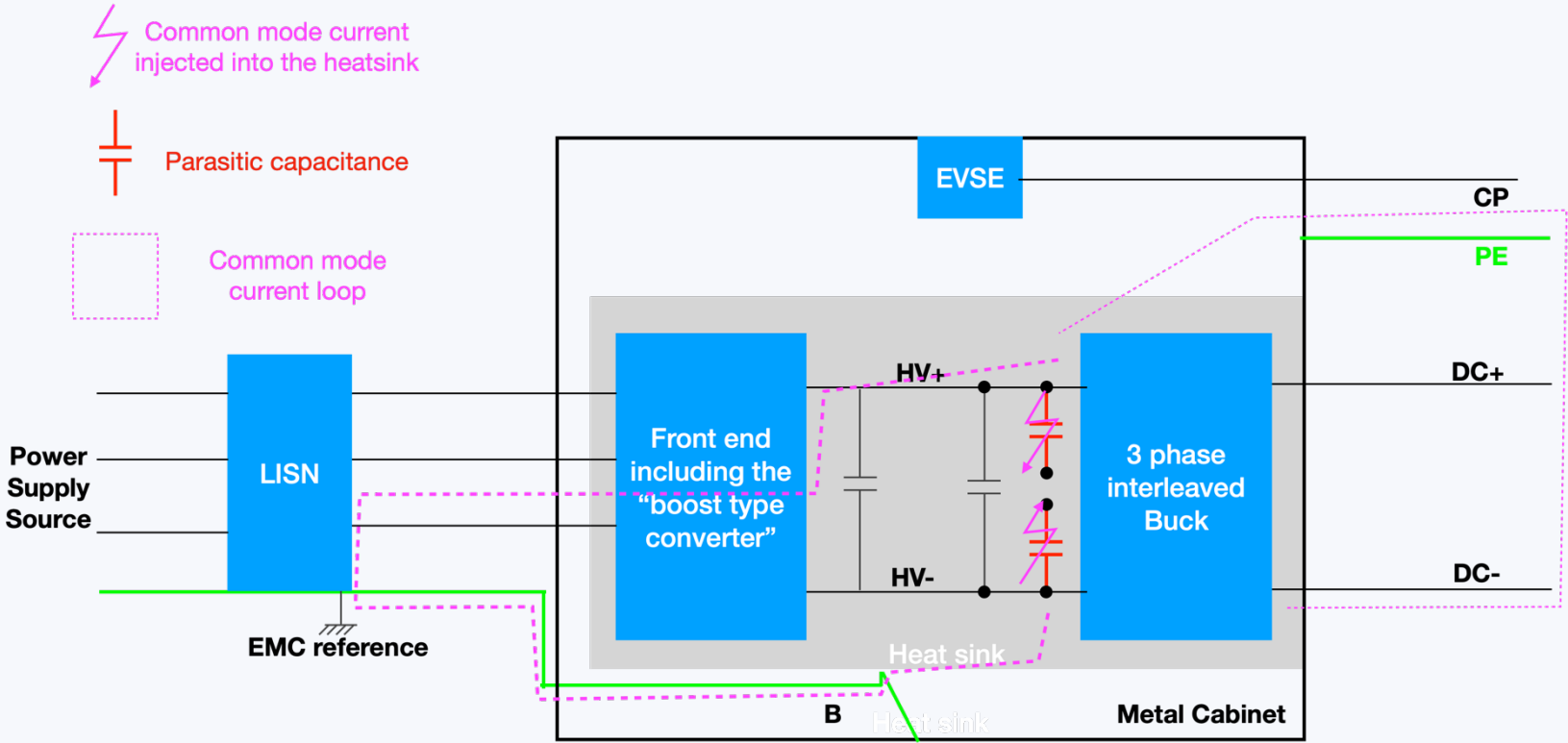
Conducted Emissions - Low-frequency Common Mode Noise



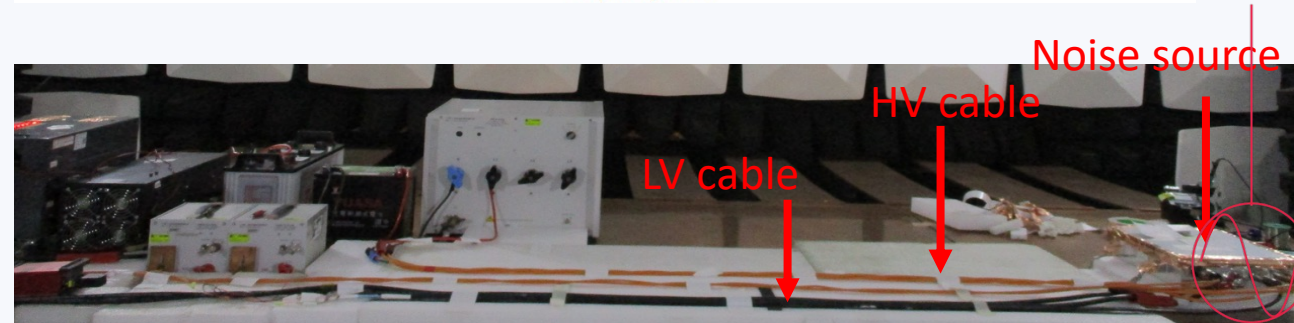
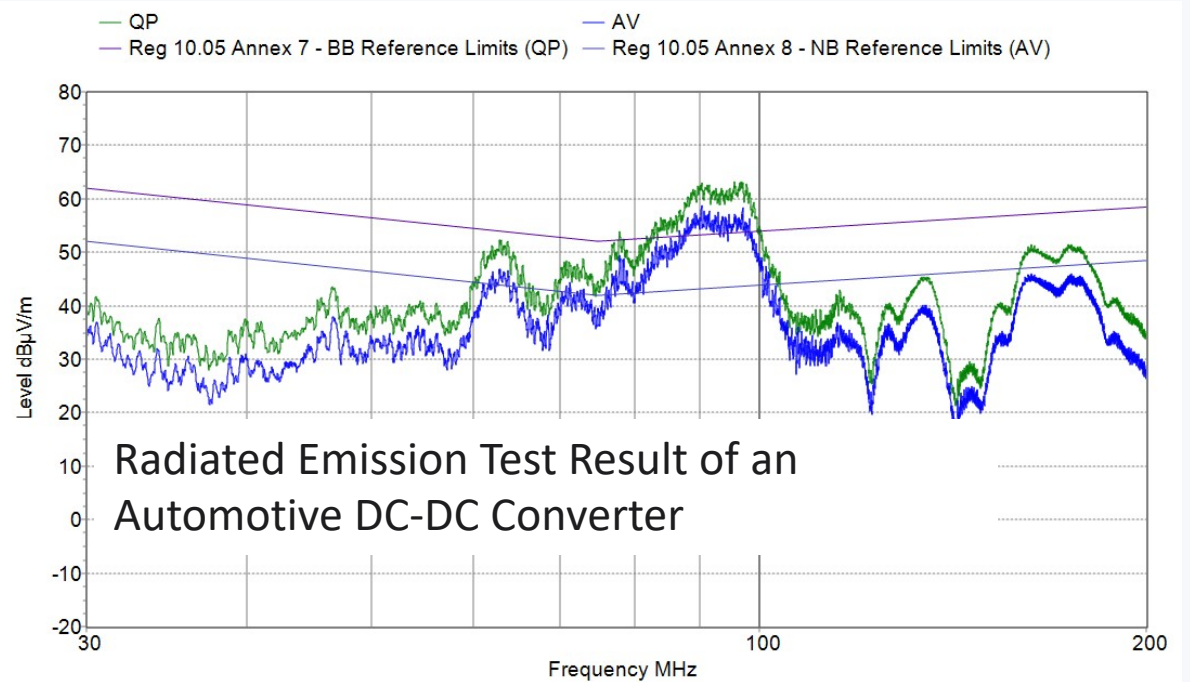
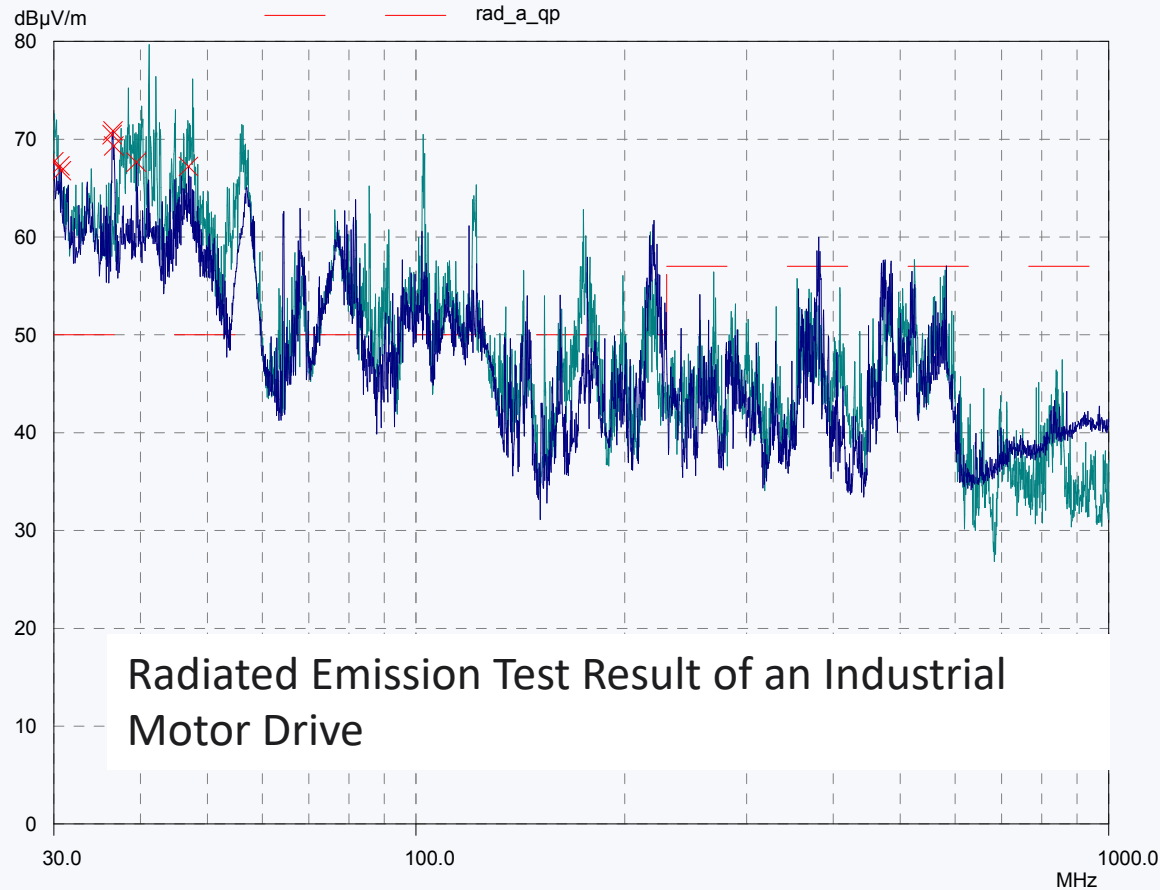
(a) the power converters are bolted to the heat sink which is earthed



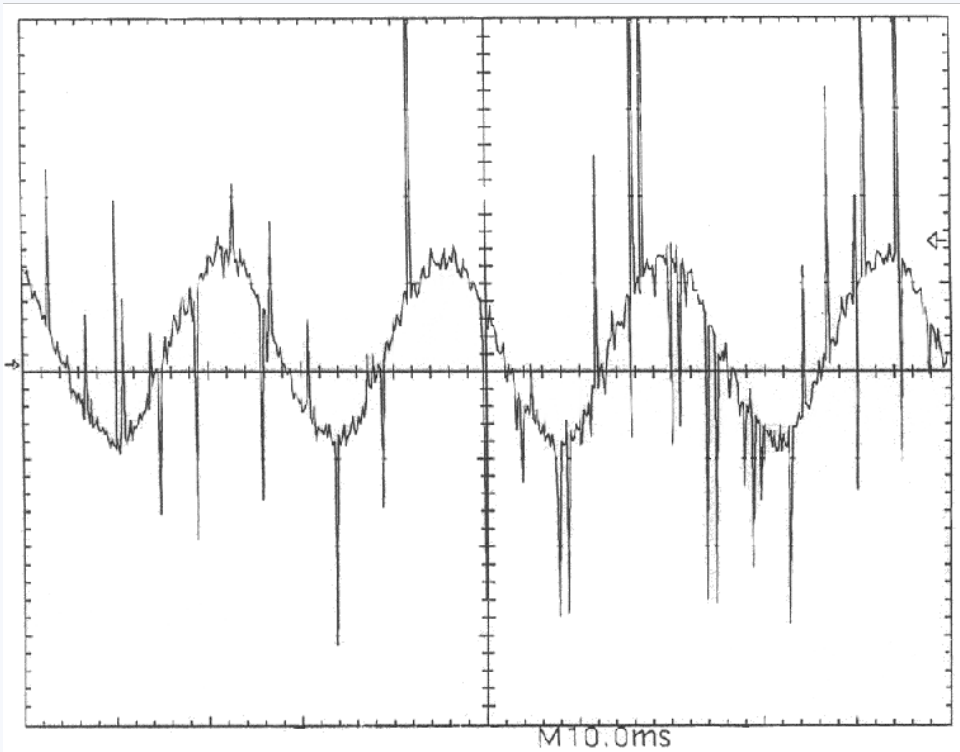
(b) A detailed view between the power switches and the heatsink



Radiated Emissions – Cables as the Main Radiators



Going Beyond Meeting Regulatory Requirements



A highly distorted current waveform of a motor
(sources: Rockwell Automation)

$$I_{ph} = I_{fundamental} + I_{harmonics} + I_{switching} + I_{transient}$$

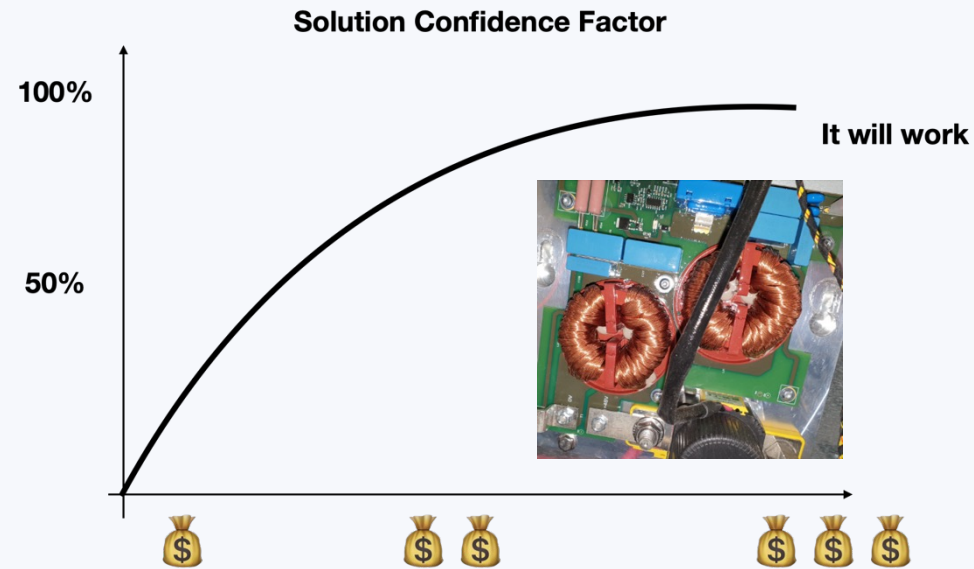
- The fundamental content depends on the motor speed.
- Low-frequency noise (kHz - 10s of kHz range) arises from the lower harmonics content of the current waveform.
- Broadband noise (30-300 MHz) is generated due to the fast rise time of the switching devices.
- High-frequency noise (>300 MHz) results from events such as reverse recovery charge of a body diode or occasional electrical breakdown caused by bearing current in an electric motor.

Insulation Breakdown, Bearing Lifetime, Sensor Inaccuracy, etc -> Functional Safety?

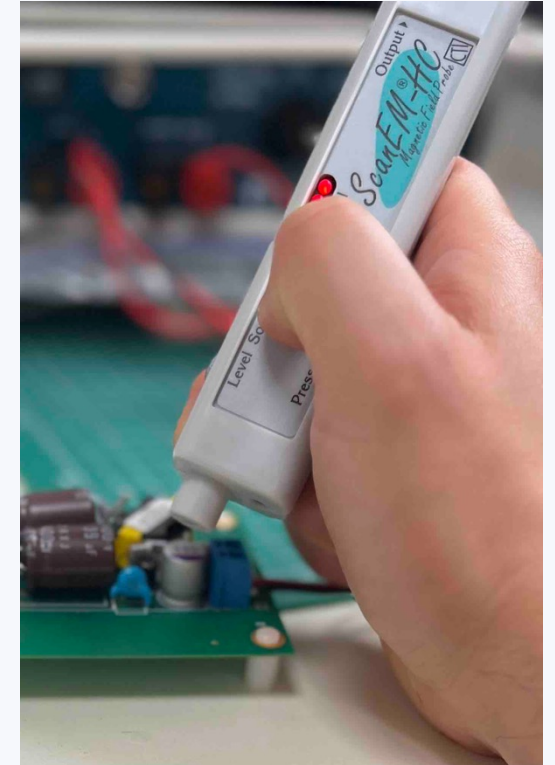
What shall we do?



Design, Develop & Pray

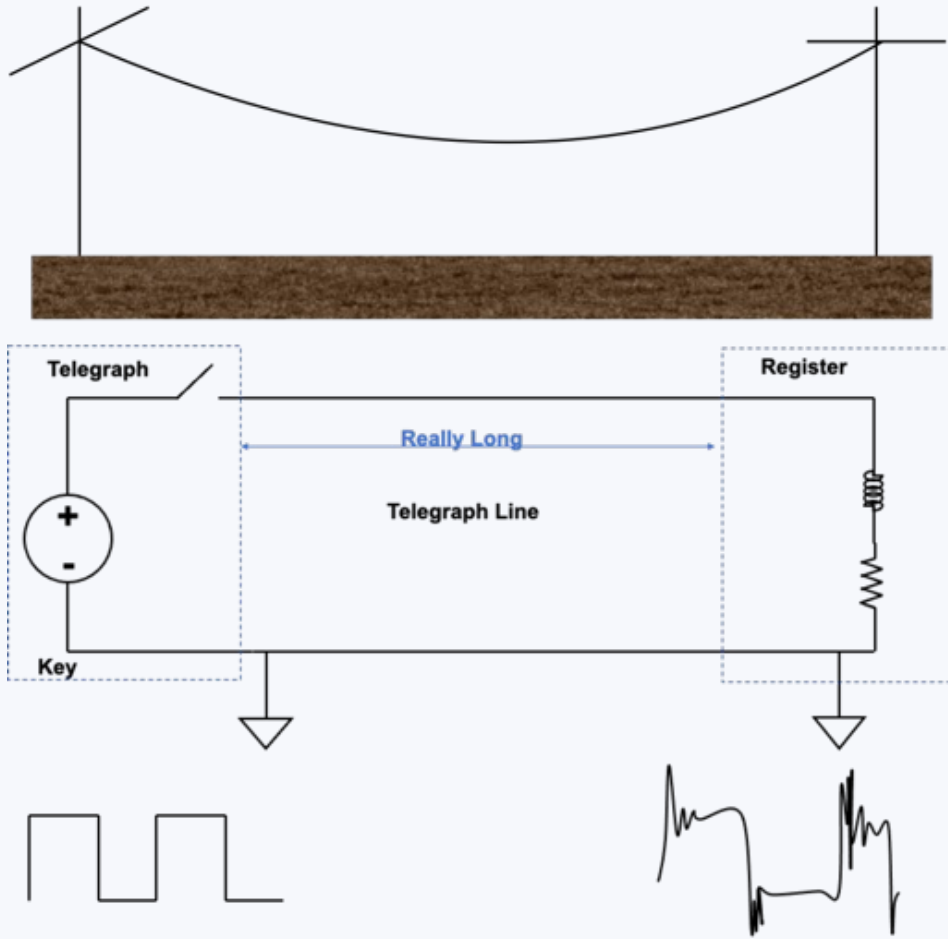


Filtering & Shielding, the More, the Better.

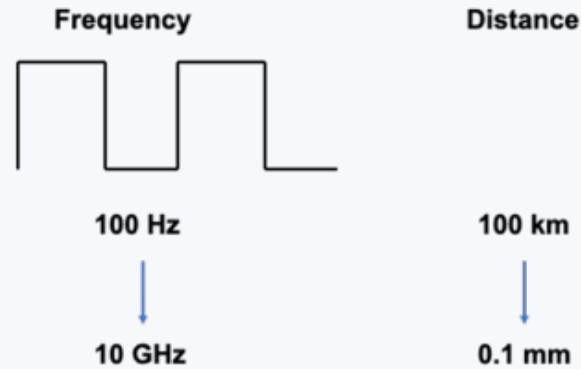
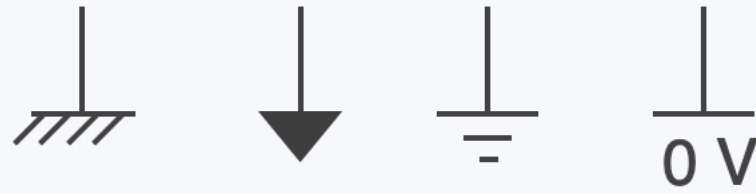


Identify, Locate & Solve

Demystifying "Ground"



A telegraph system that Samuel Morse built



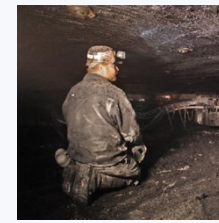
Sending a GHz signal on a PCB is, electromagnetically speaking, almost like sending a Morse code across the country.

As a rule of thumb, if the device you are transmitting electric signals across is larger than 1/10 of a wave length, then you need to start thinking about transmission line theory.



An FPGA chip on the PCB

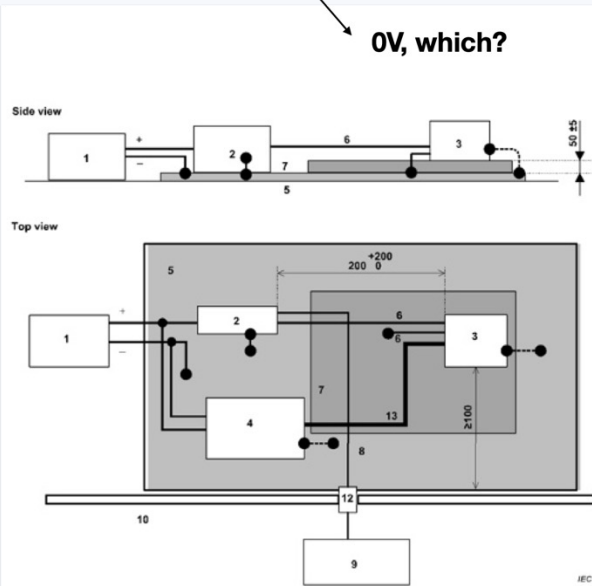
Searching for a “Quiet Ground”



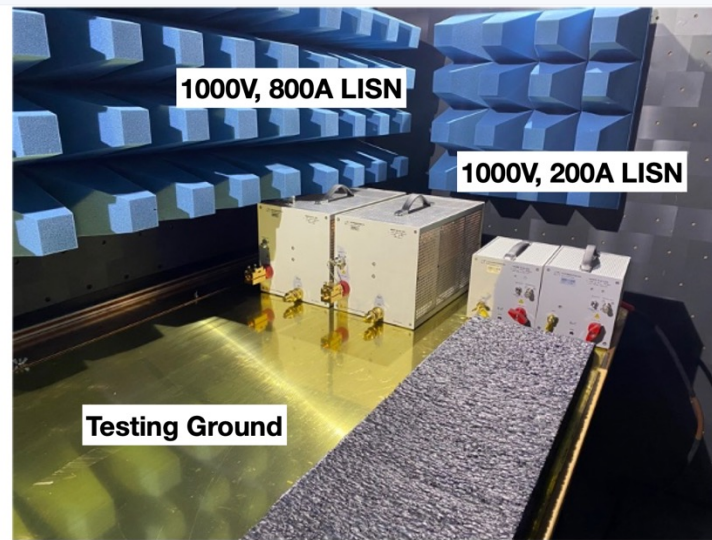
- Often referred to as “Reference Ground Plane”
- Made of copper, brass, bronze or galvanised steel, the ground plane is the top metallic surface on the test bench/table and electrically bonds to the walls or the floor of the shielded enclosure such that its DC resistance does not exceed 2.5 mΩ.
- Conducted emission is to measure the noise with respect to the “reference ground plane” or “Ground plane”.

Where is the “ground”?

- The quiet “ground” ?
- The RF reference point ?
- The earth?
- 0V, which?



For automotive applications, the “ground” is the negative end of the 12V battery, which is connected to the vehicle chassis.

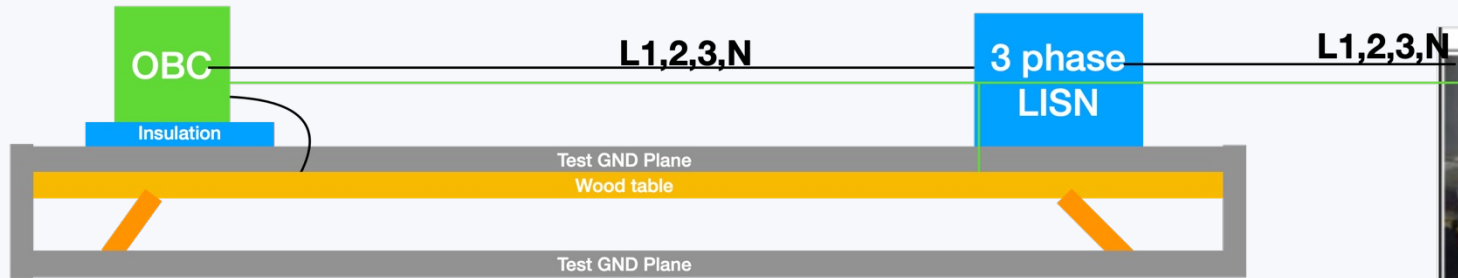


Conducted emissions set-up - CISPR 25



A popular milli-ohmmeter used for checking the continuity of the ground plane and LISN connections

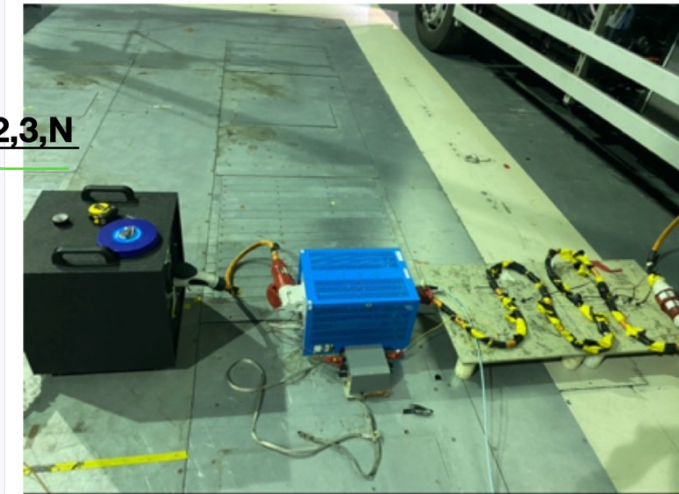
The On-Board Charger “Ground” Puzzle



Component test - The test ground plane is connected to the 3-phase LISN, with the PE wire connected; eventually, this ground plane is connected to Earth.



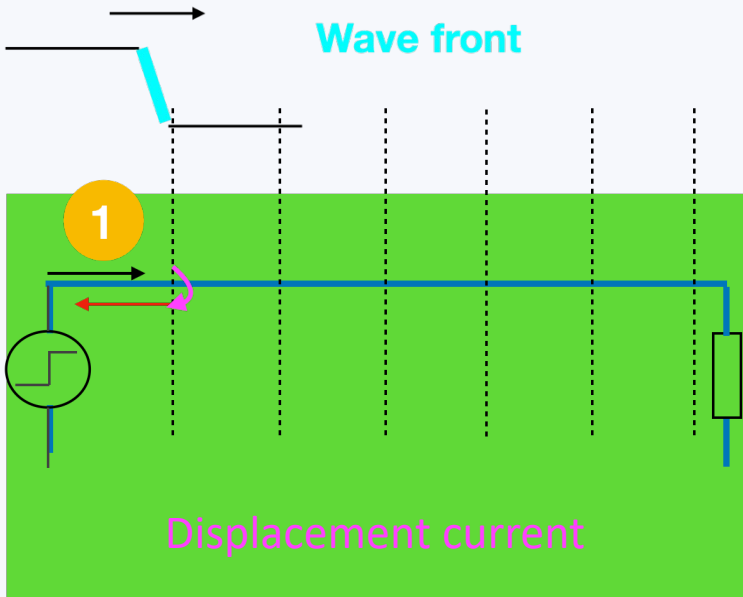
Vehicle test - Very similar to the component test, but there is no electrical connection between the vehicle chassis and the test ground plane. The vehicle chassis cannot be compared with a test ground plane (in terms of conductivity) either.



The Return Current Path

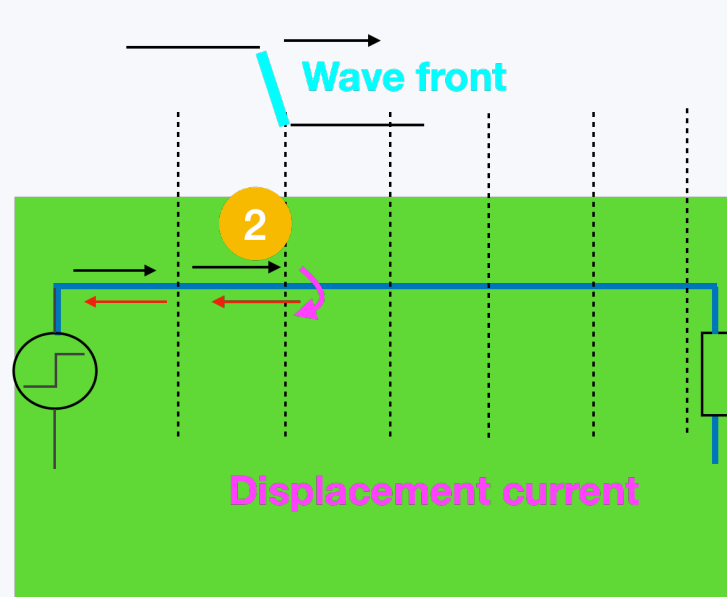
Wave propagation

Wave front

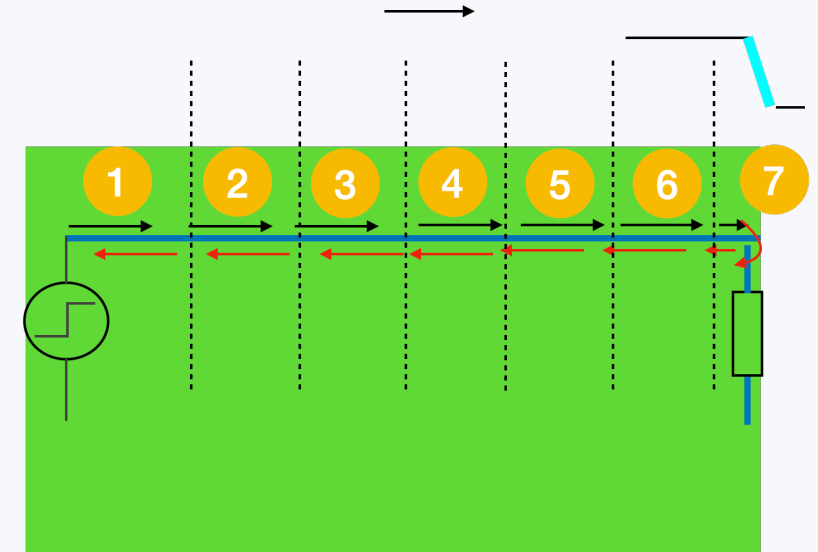


Wave propagation

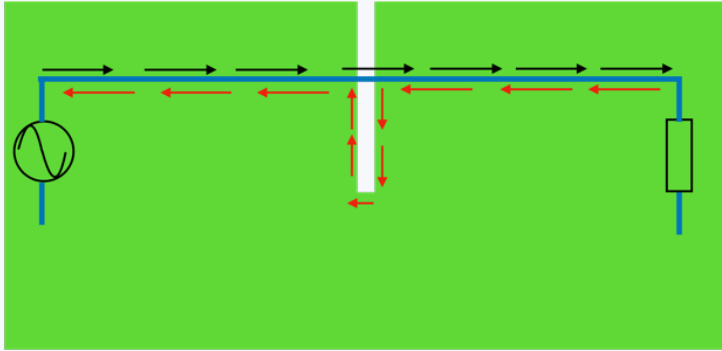
Wave front



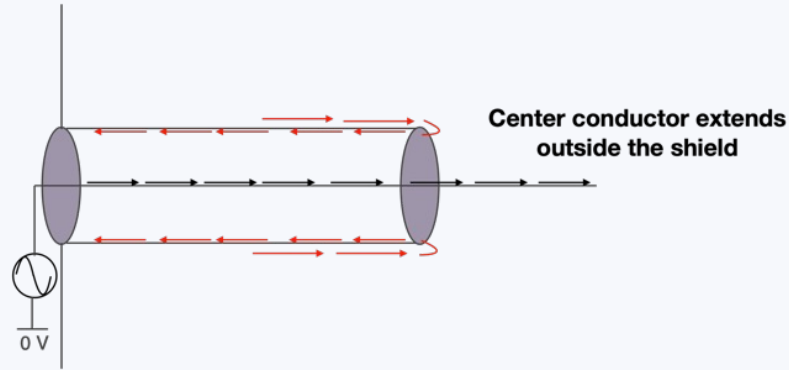
Wave propagation



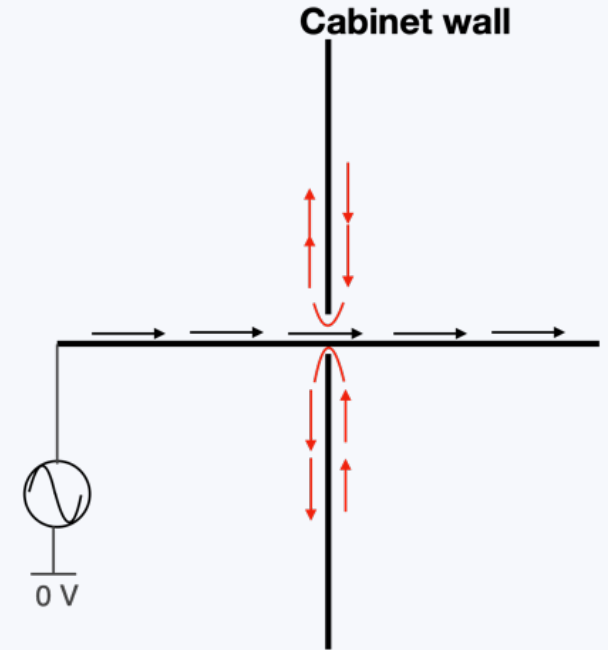
Common “Ground” Issues



Ground plane break



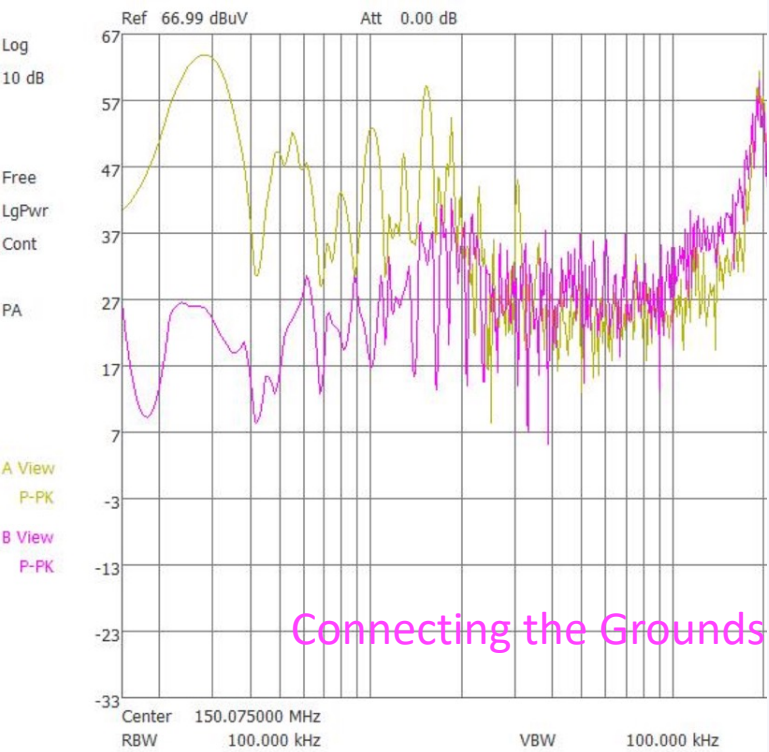
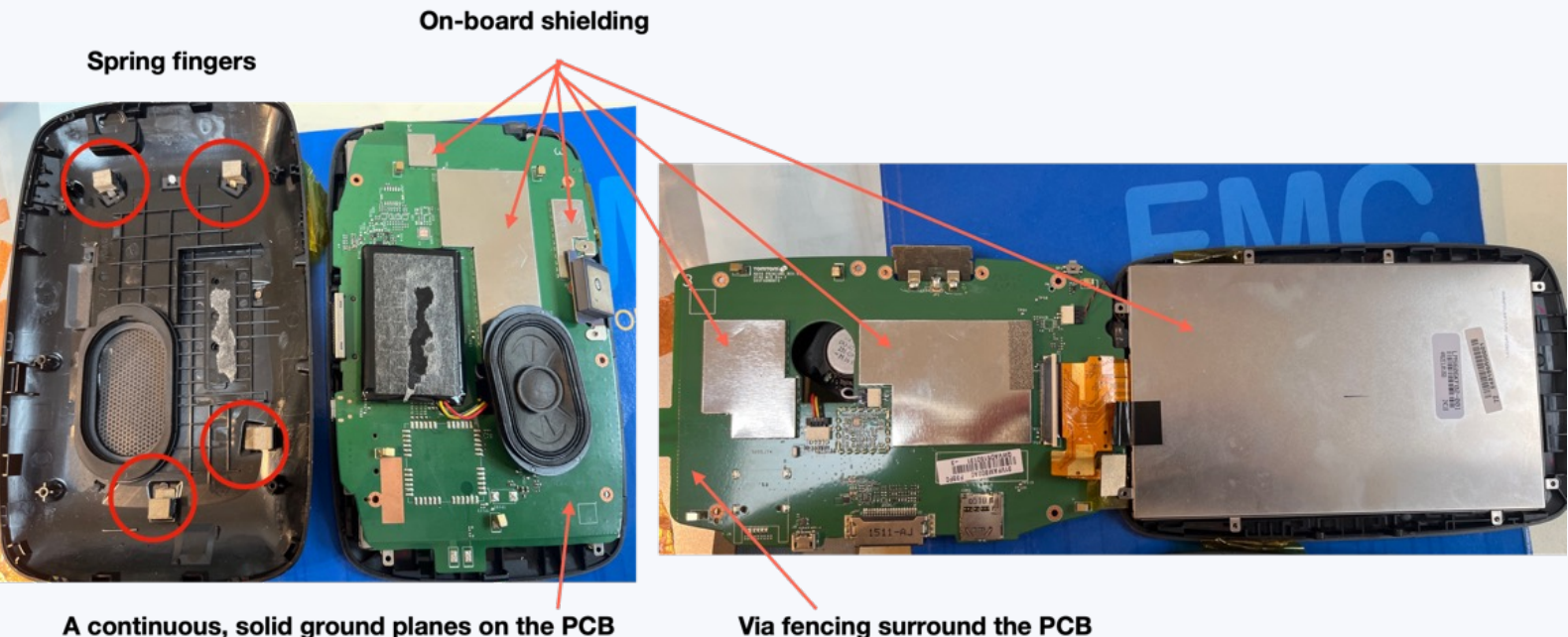
Conductor extends outside the shield



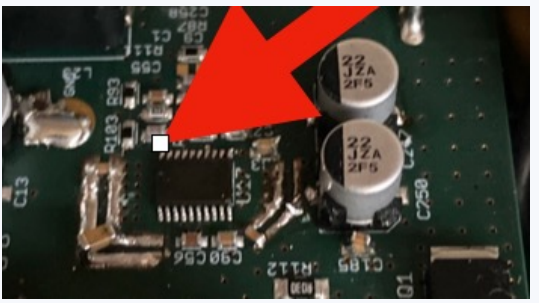
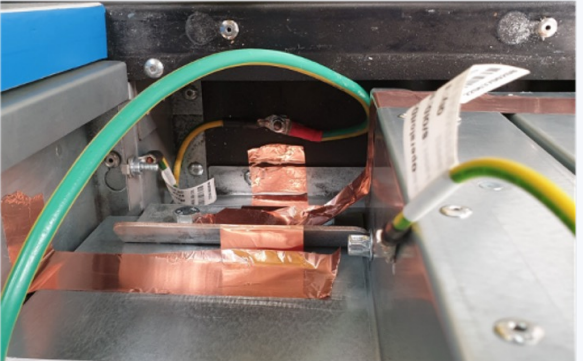
Wires penetrating into an enclosure

- Ferrite/Magnetic core has no improvement in emissions.
- Capacitors to chassis (common mode caps) make no difference/make things worse.
- “Balloon effect”
- Ineffective shielding
- Susceptible to immunity issues

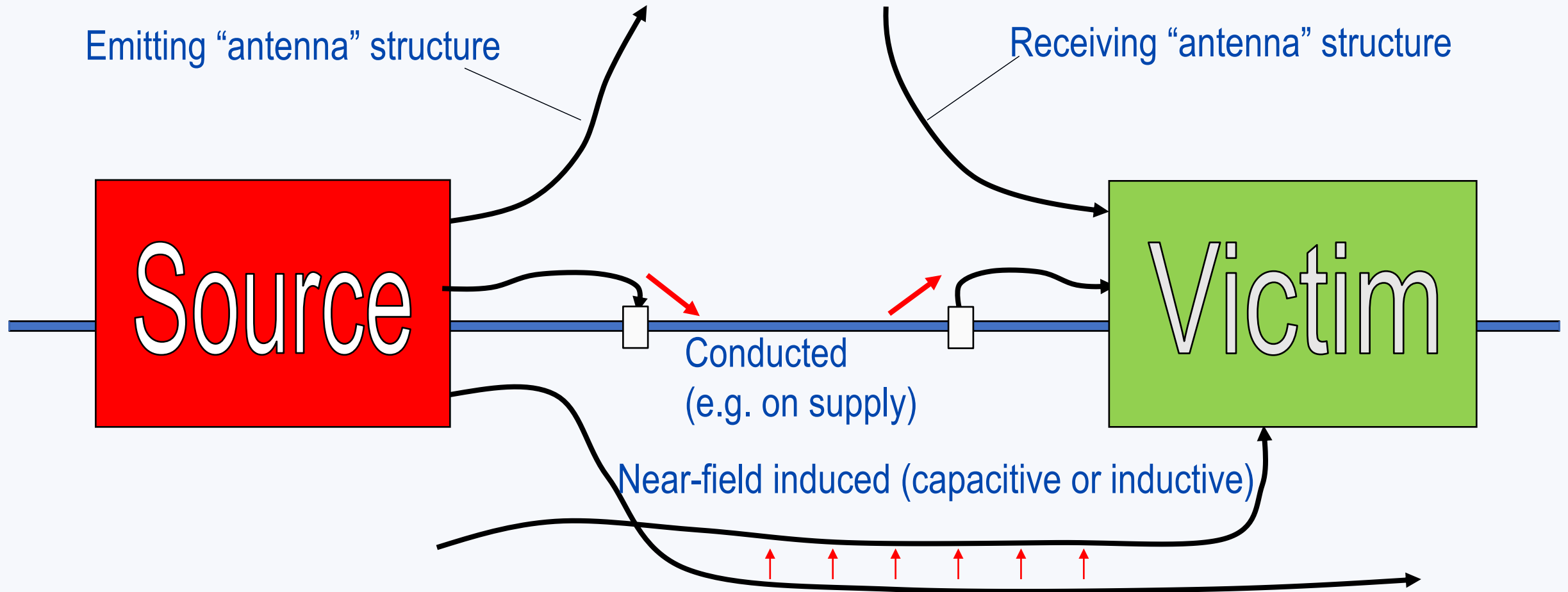
We Need One Ground and One Ground Only



Connecting the Grounds

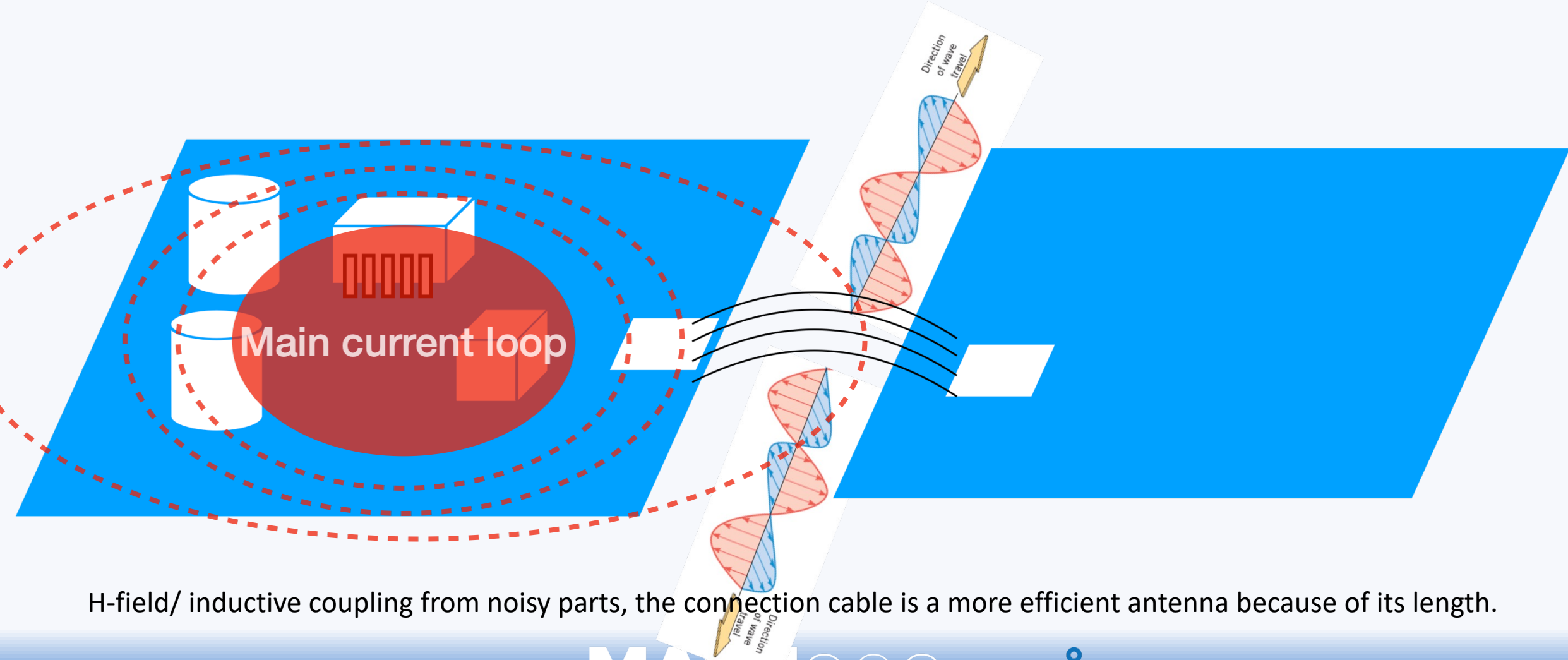


Coupling Mechanism



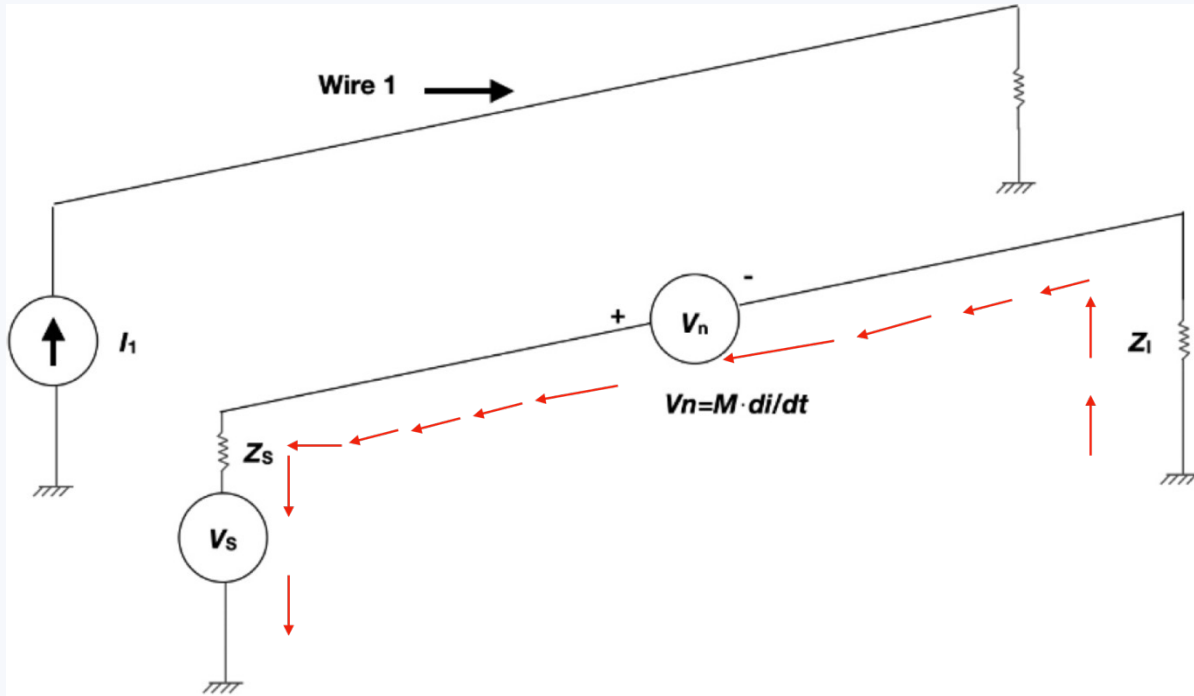
Source: T. Williams "EMC for Product Designers"

Near-field coupling: Magnetic Field/Inductive Coupling



H-field/ inductive coupling from noisy parts, the connection cable is a more efficient antenna because of its length.

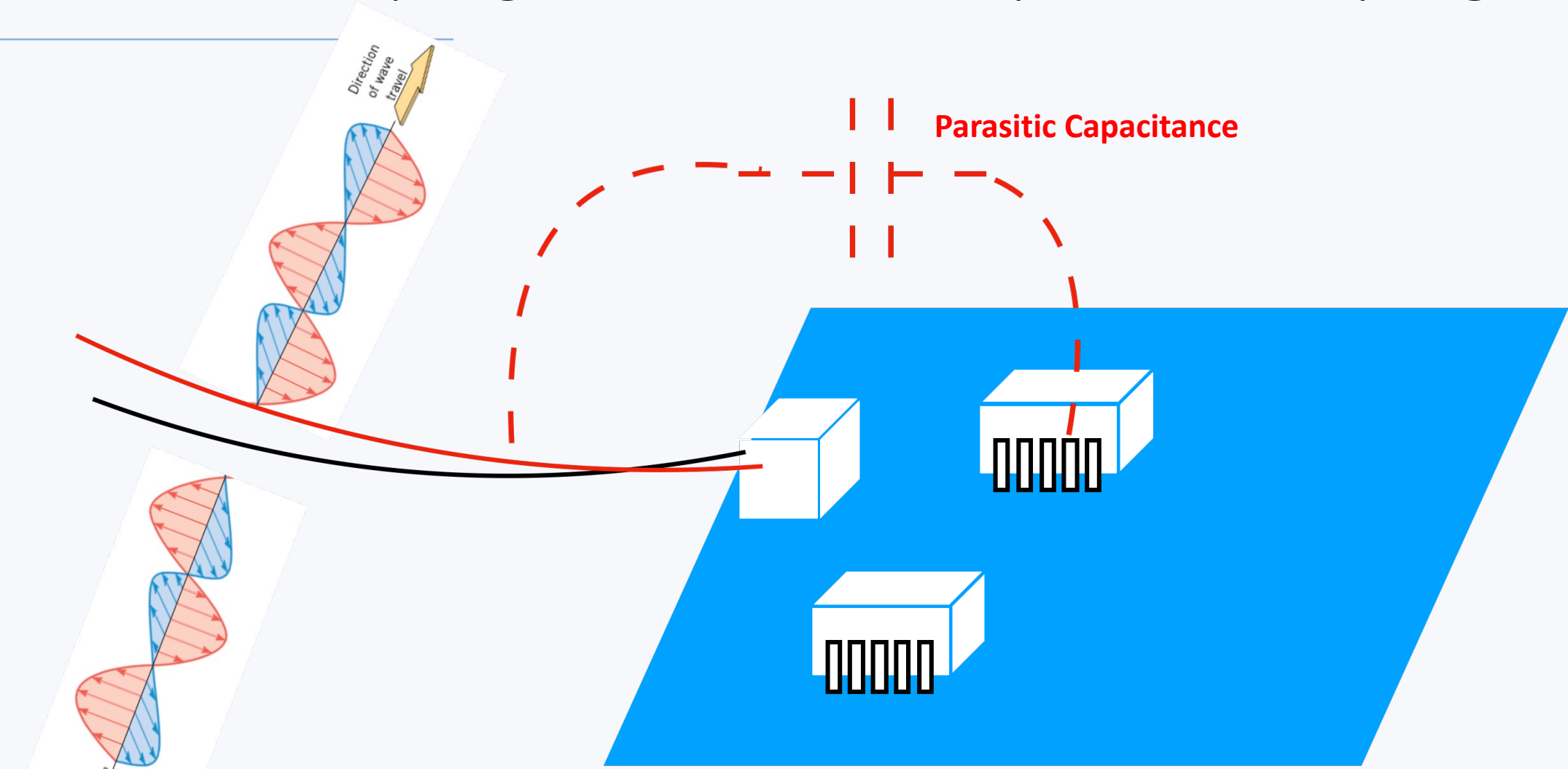
Near-field coupling: Magnetic Field/Inductive Coupling



- Two conductors represent two parallel run wires, traces over a PCB, etc.
- Ignoring the capacitance effect in this example.
- I_1 represents the noise source, in this case, it is a current source.
- What is the induced interference voltage on Z_l ?

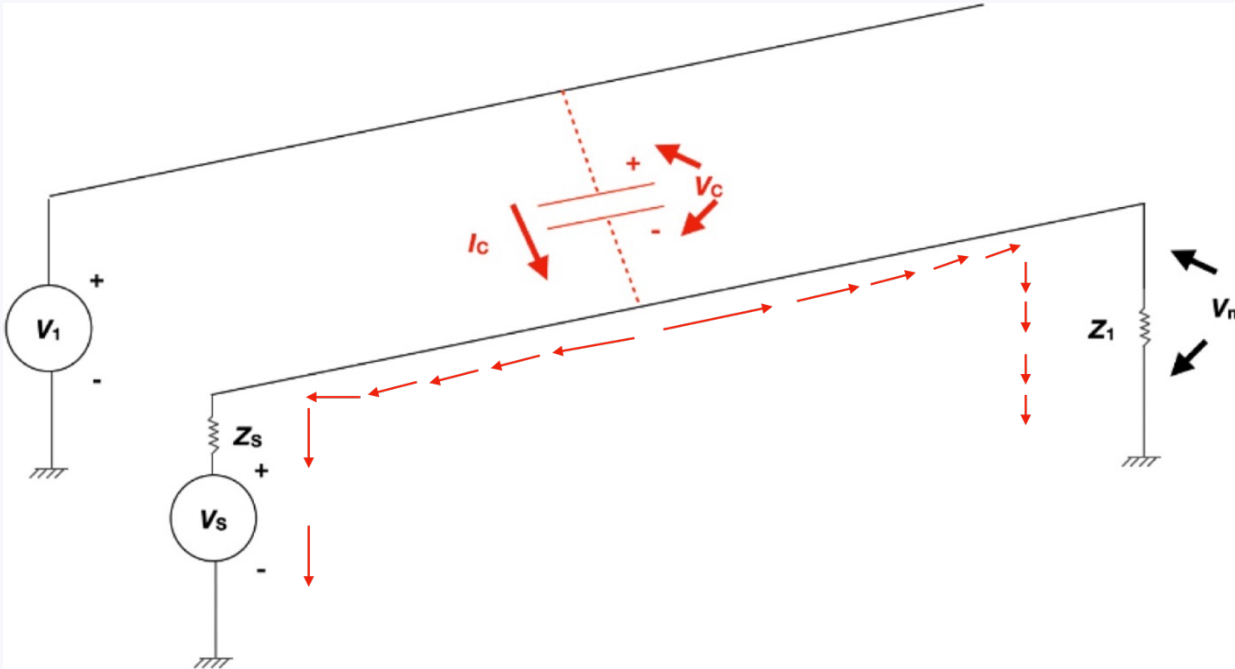
$$V_l = M \frac{dI_1}{dt} \frac{Z_l}{Z_s + Z_l}$$

Near-field coupling: Electric Field/Capacitive Coupling



E-field/ Capacitive coupling from noisy parts, the input cable is a more efficient antenna because of its length.

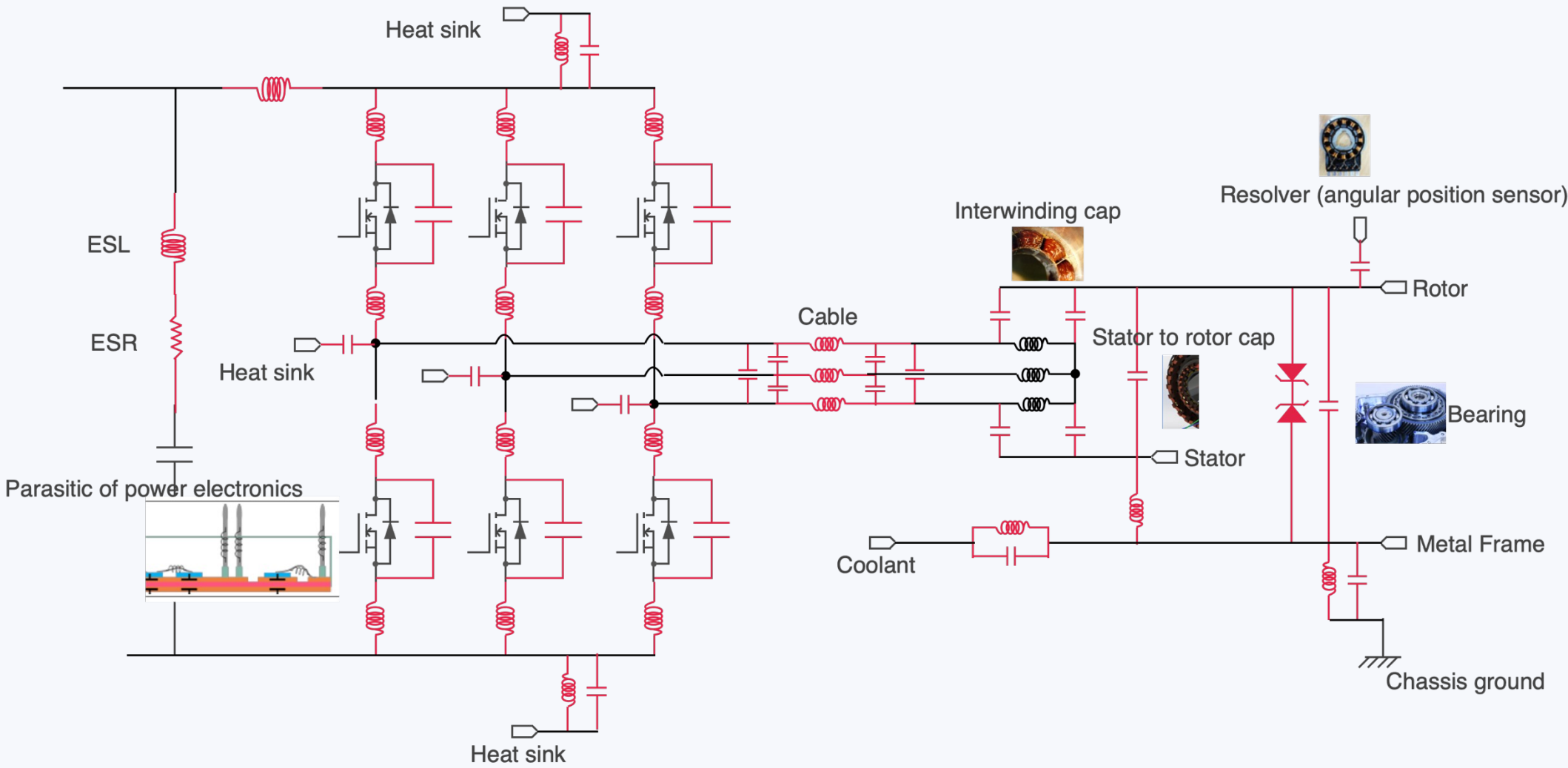
Near-field coupling: Electric Field/Capacitive Coupling



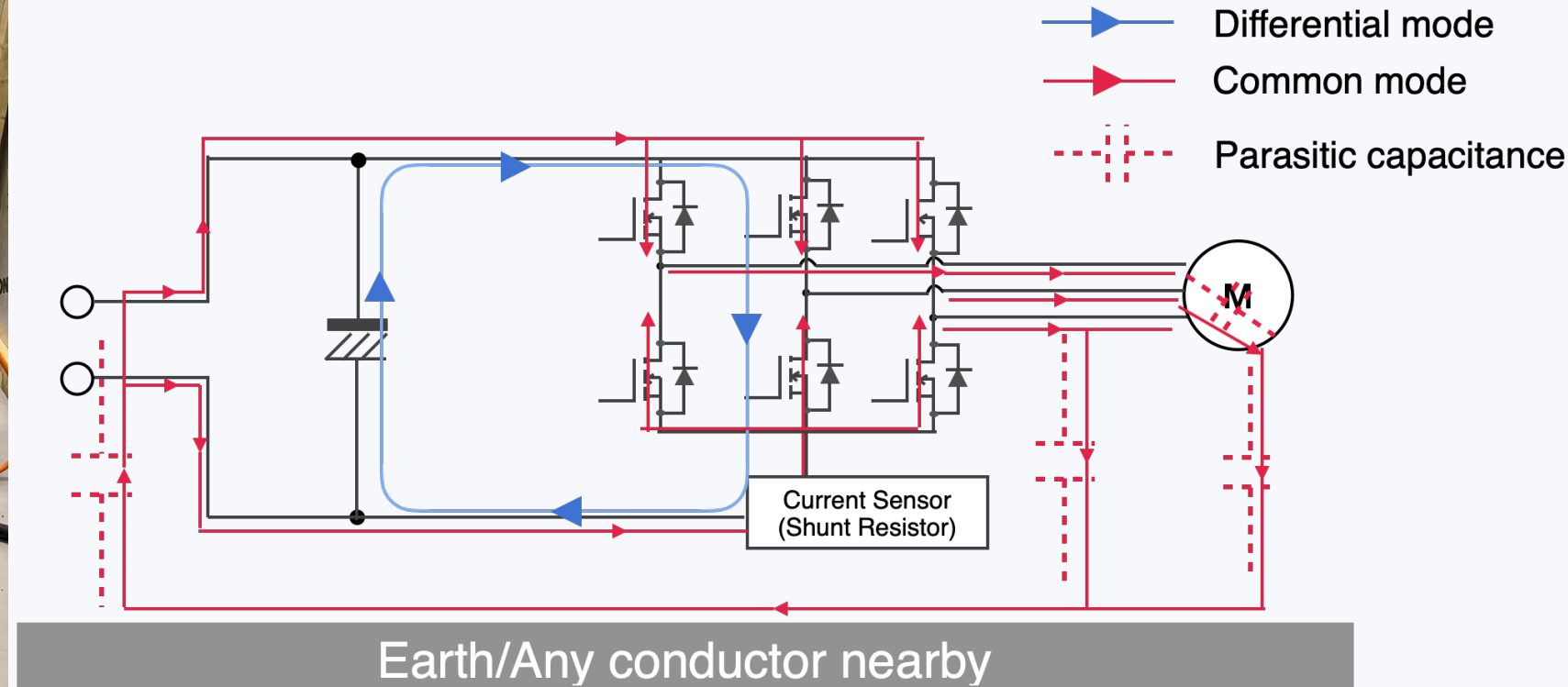
- Two conductors represent two parallel run wires, traces over a PCB, etc.
- Ignoring the inductance effect in this example.
- V_1 represents the noise source.
- What is the induced interference voltage on Z_1 ?

$$V_n = C \frac{dV_1}{dt} (Z_s || Z_l)$$

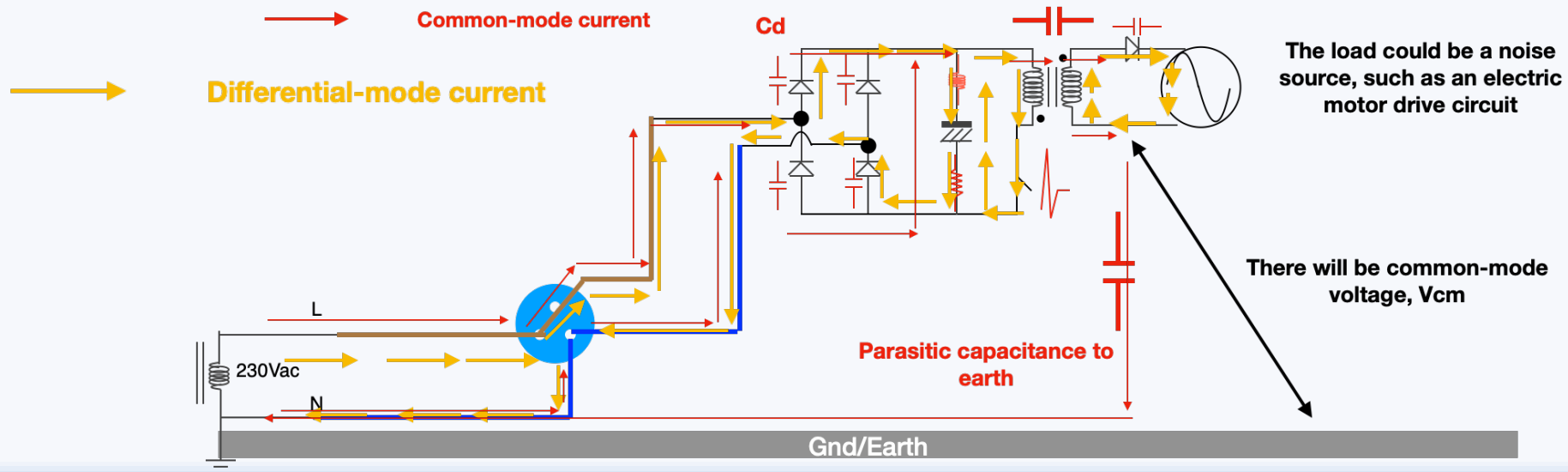
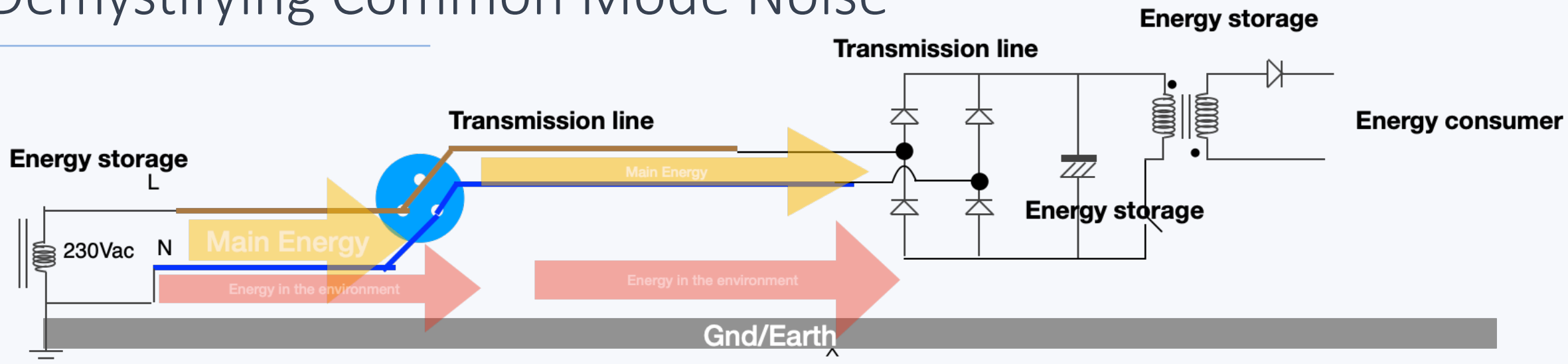
Understanding Coupling and Parasitics



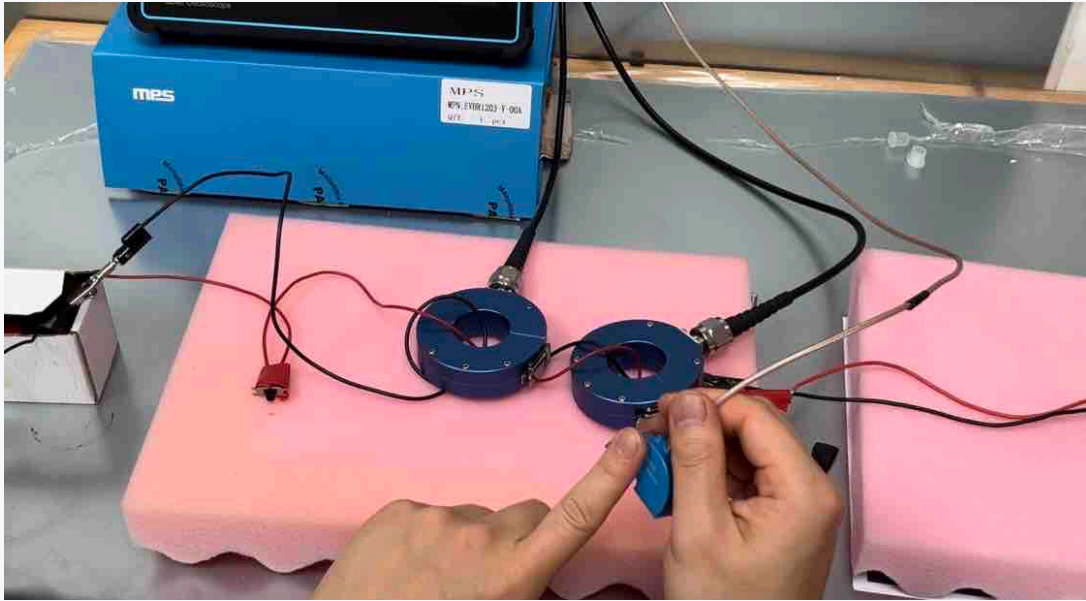
Understanding Coupling and Parasitics:



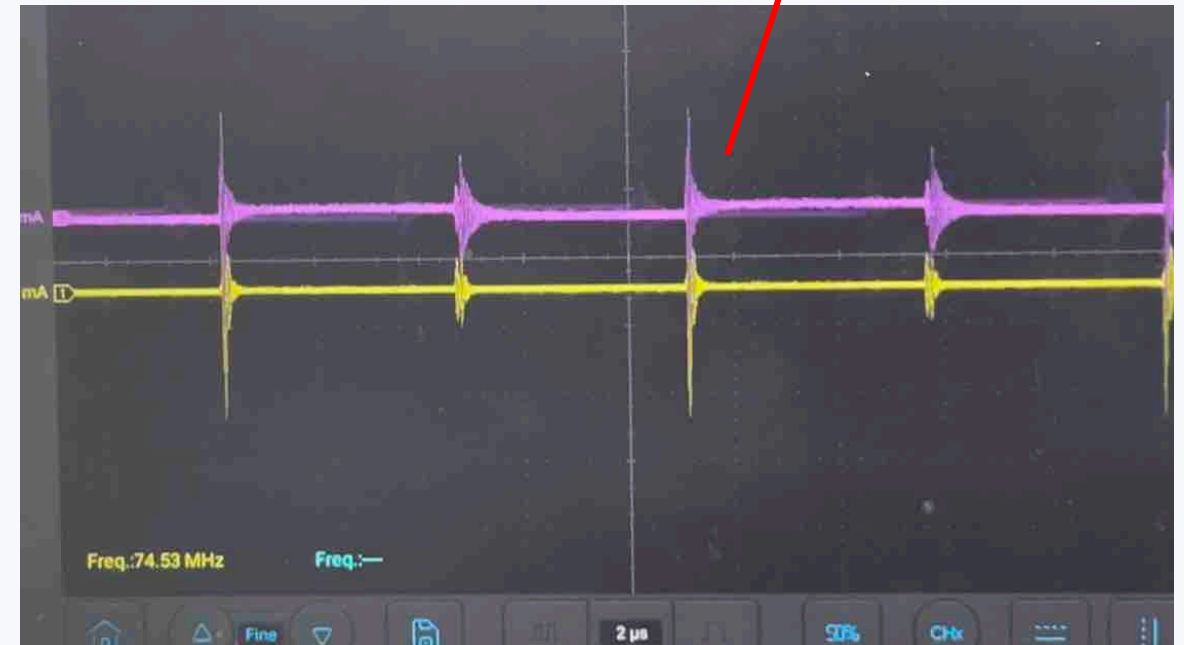
Demystifying Common Mode Noise



Measuring the Common Mode Noise



Using RF current probes

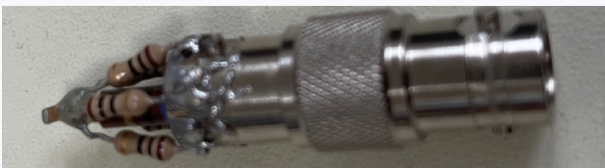
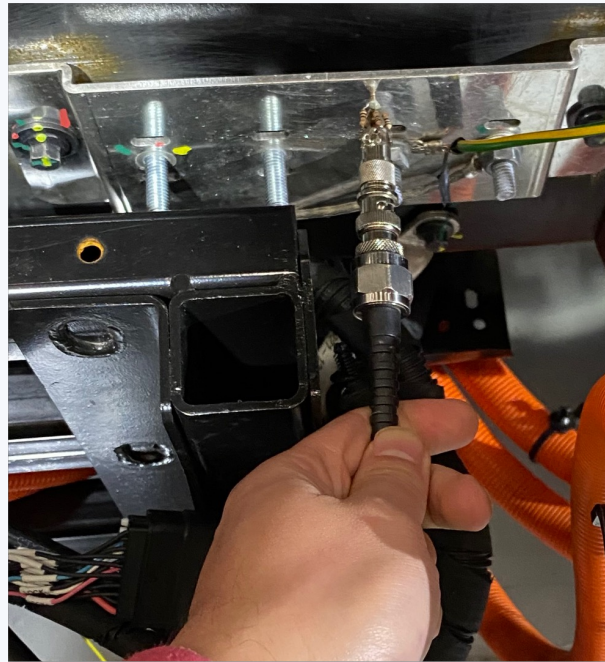


Forward common mode current and return current

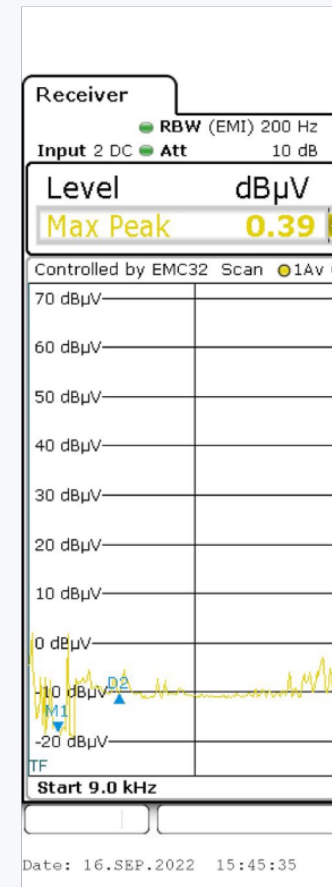
Measuring the Common Mode Noise



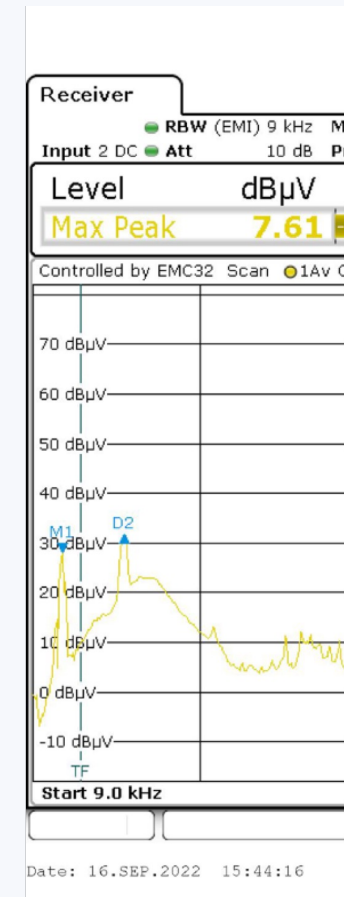
Measuring surface currents on the vehicle chassis



A home-made resistive probe



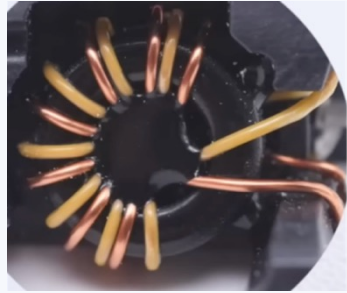
(a) when the OBC was off



(b) when the OBC was on

The surface noise was measured in the low-frequency range

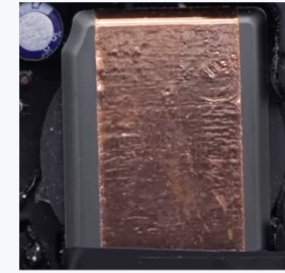
Understanding Coupling and Parasitics: The Key to Designing EMC Filters



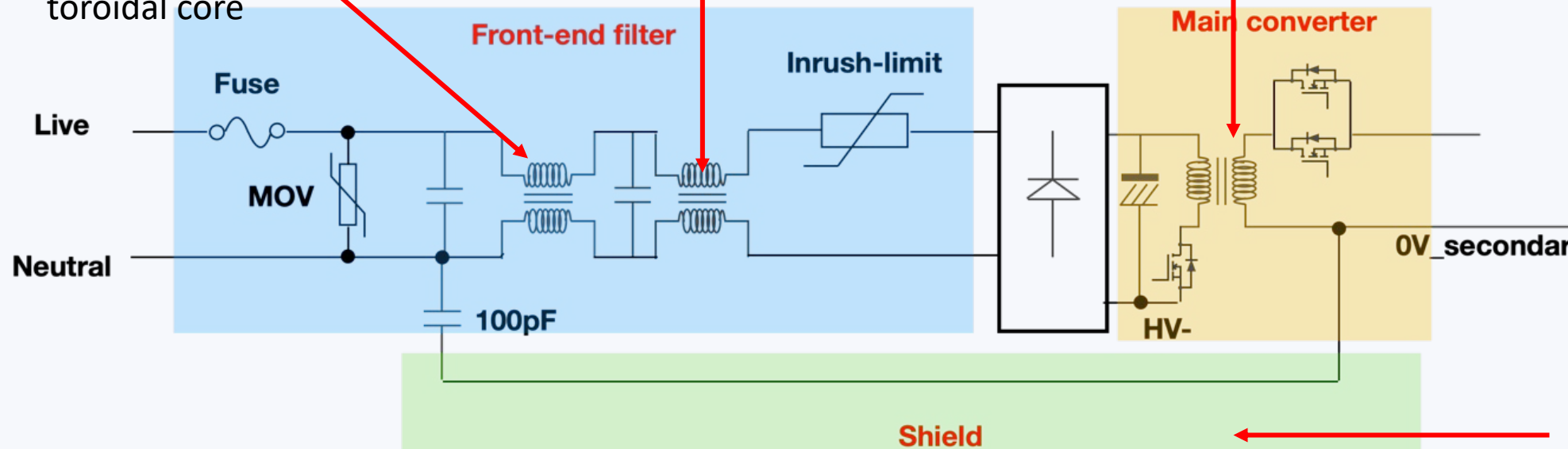
Bifilar winding on a toroidal core



Flat-wire winding on a sectional wound CMC



A magnetic flux band around the transformer



A simplified isolated power supply circuit using GaN devices

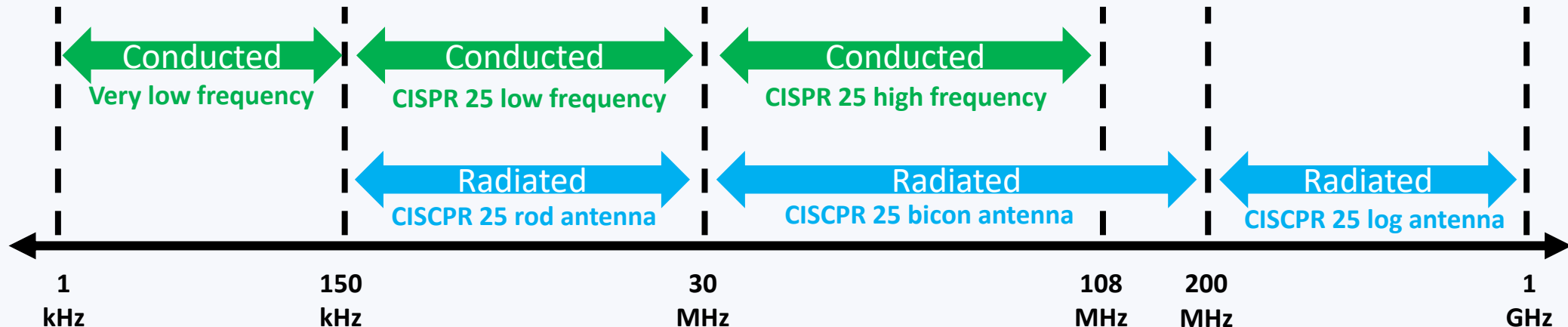
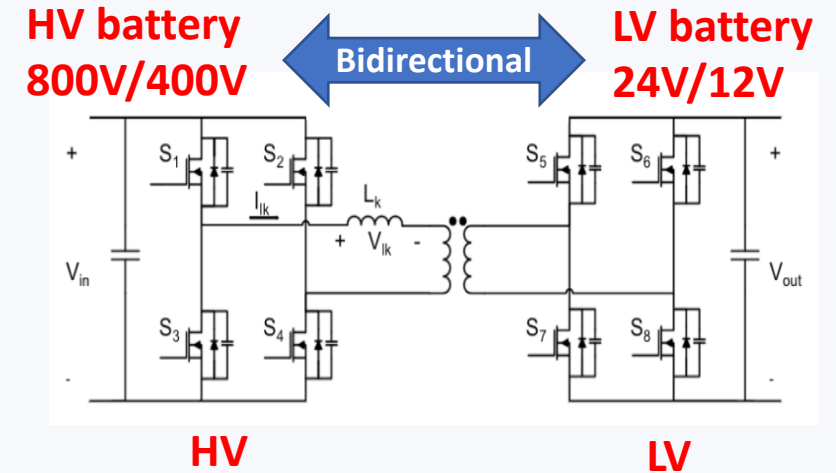
Benchtop EMC Testing

EMI can no longer be an after thought!

- CISPR 25 Automotive EMC standard
 - Conducted Emissions: 150kHz-108MHz
 - Radiated Emissions: 30MHz-2.5GHz



Lyra's 4kW SiC DC-DC Converter

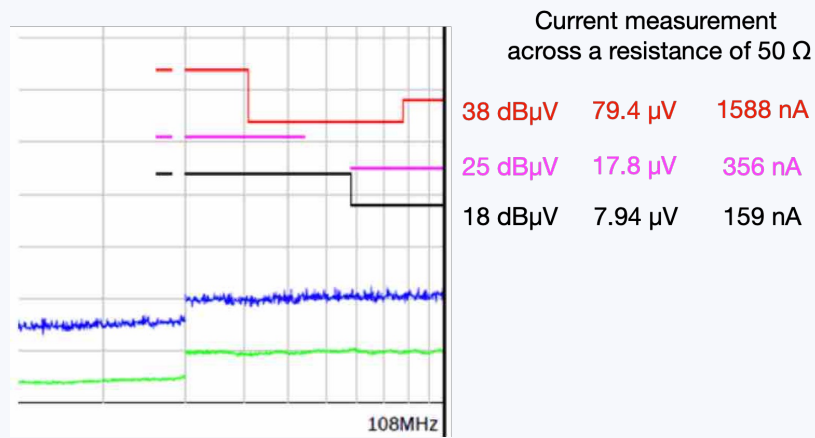


CISPR 25 Testing Methods

- CISPR25 defines two methods for conducted emissions testing:
 - Current probe method
 - Voltage method.
- Both methods can be used to determine if the device under test (DUT) passes or fails the emission test limits.
- Test method is defined by the OEM requirements.

Table 1. CISPR25 Class 5 Peak Limits for Voltage Method and Current Probe Method

Frequency (MHz)	Voltage Method (dB μ V)	Current Probe Method (Converted to dB μ V)
0.15 to 30	70	84
0.53 to 1.8	54	60
5.9 to 6.2	53	53
76 to 108	38	38
26 to 28	44	44
30 to 54	44	44
68 to 87	38	38



This is the limit for a 48-12V DC-DC which often has a power of 700W. But it is exactly the same limit for a 600V-12V DC-DC which has a power of 3kW, same limit for an electric motor whose power exceeds 250 kW.

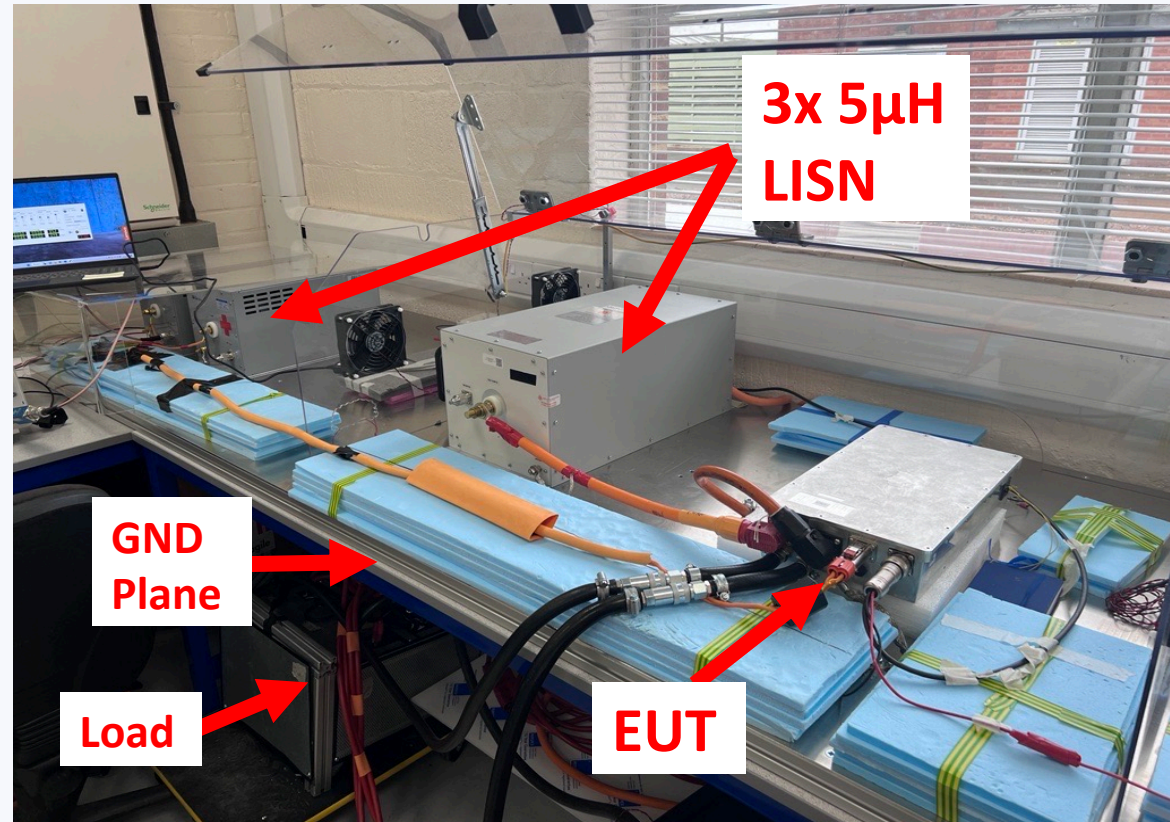
CISPR 25 Conducted Emissions Test Setup



- 7 Low relative permittivity support ($\epsilon_r \leq 1,4$)
- 8 High-quality coaxial cable e.g. double-shielded (50Ω)

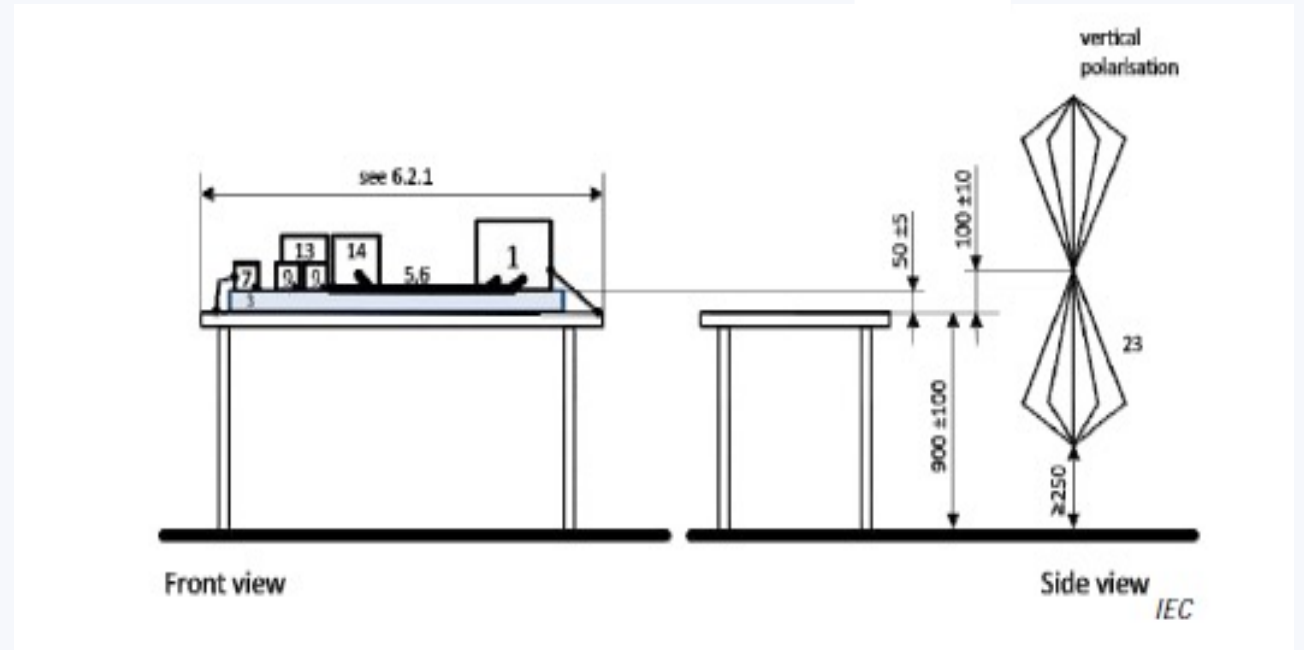
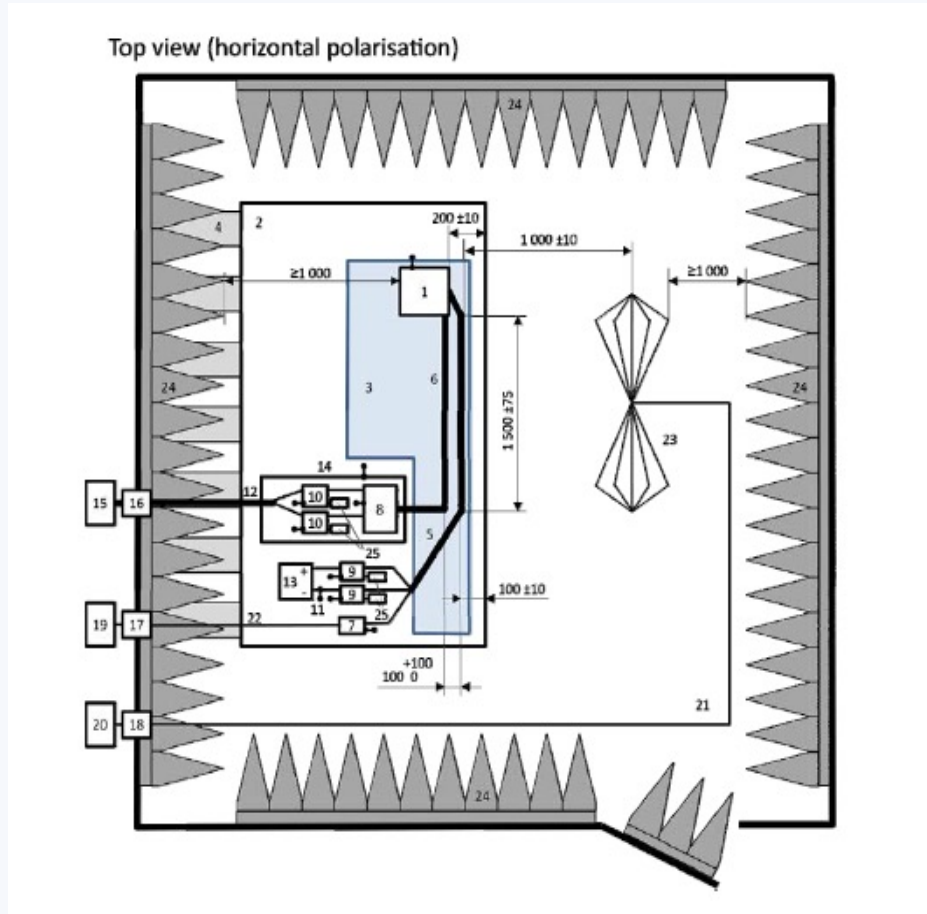
EUT with power return line locally grounded

[1] CISPR 25:2016 © IEC 2016



Test setup at Lyra

CISPR 25 Radiated Emissions Test Setup

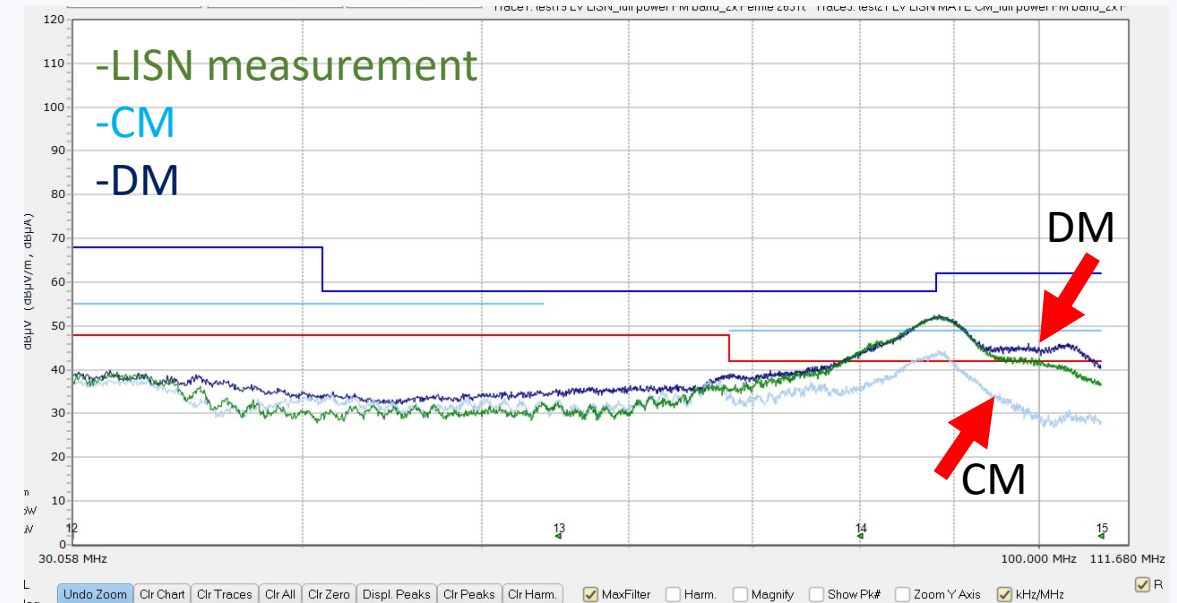
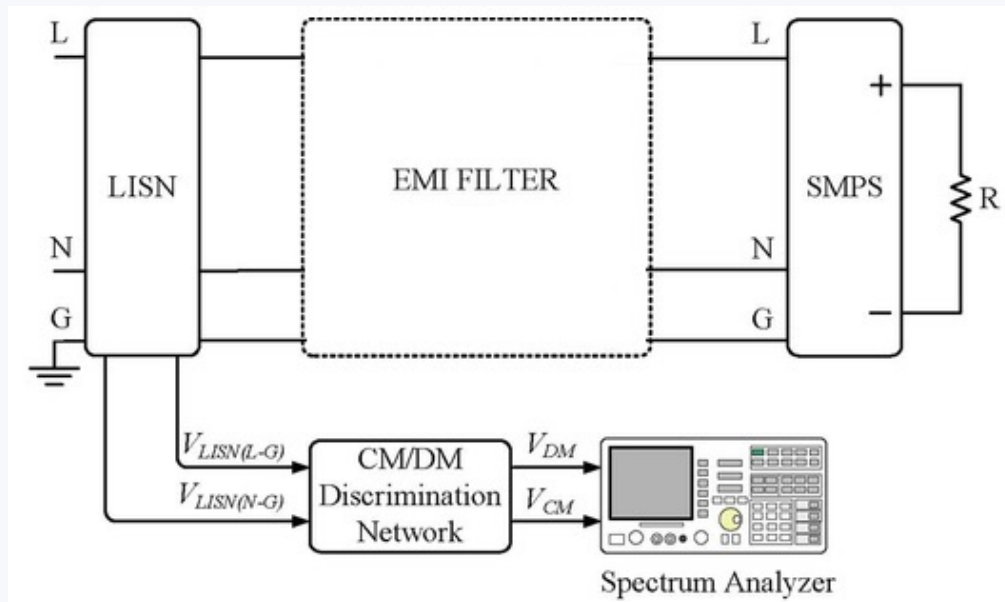


Key

- | | | | |
|----|---|----|--|
| 1 | EUT | 14 | Additional shielded box |
| 2 | Reference ground plane | 15 | HV power supply (should be shielded if placed inside ALSE) |
| 3 | Low relative permittivity support ($\epsilon_r \leq 1,4$) thickness 50 mm | 16 | Power line filter |
| 4 | Ground straps (see 6.2.1) | 17 | Fibre optic feed through |
| 5 | LV harness | 18 | Bulk head connector |
| 6 | HV lines (HV+, HV-) | 19 | Stimulating and monitoring system |
| 7 | LV load simulator | 20 | Measuring instrument |
| 8 | Impedance matching network (optional) | 21 | High quality coaxial cable e.g. double shielded (50 Ω) |
| 9 | LV AN | 22 | Optical fibre |
| 10 | HV AN | 23 | Biconical antenna |
| 11 | LV supply lines | 24 | RF absorber material |
| 12 | HV supply lines | 25 | 50 Ω load |
| 13 | LV power supply 12 V / 24 V / 48 V (should be placed on the reference ground plane) | | |

Measurement of Conducted Emissions with LISNs (CM & DM)

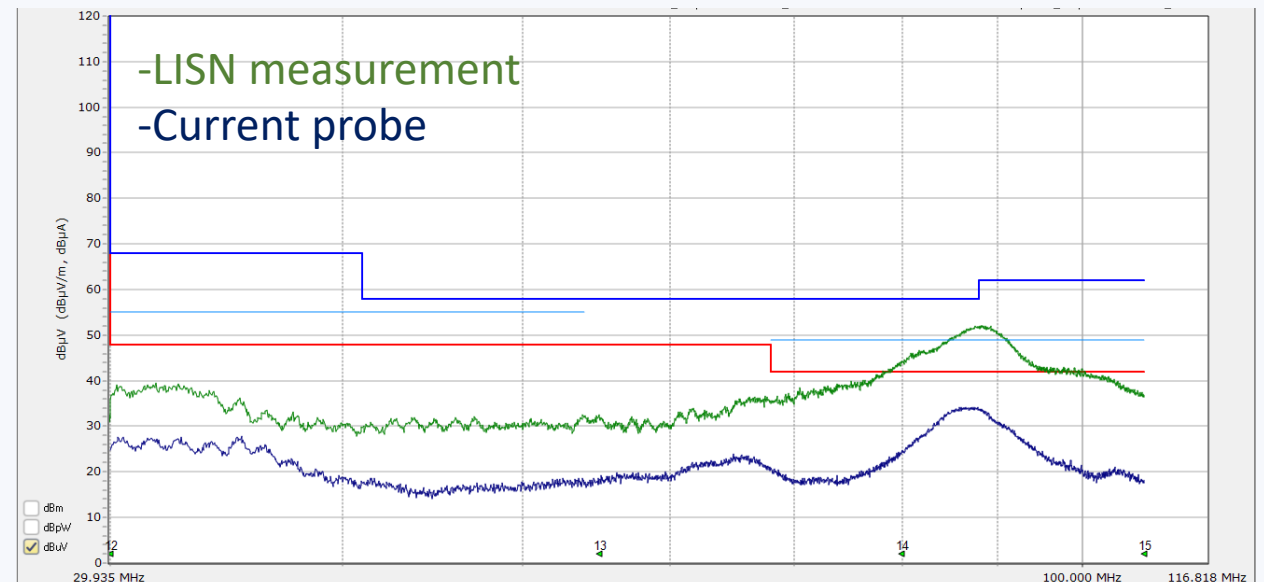
- Spectrum analyser cannot distinguish between differential mode and common mode noise.
- CM/DM discrimination network can be placed between the LISN and the spectrum analyser to separate the differential mode voltage and the common mode energy.



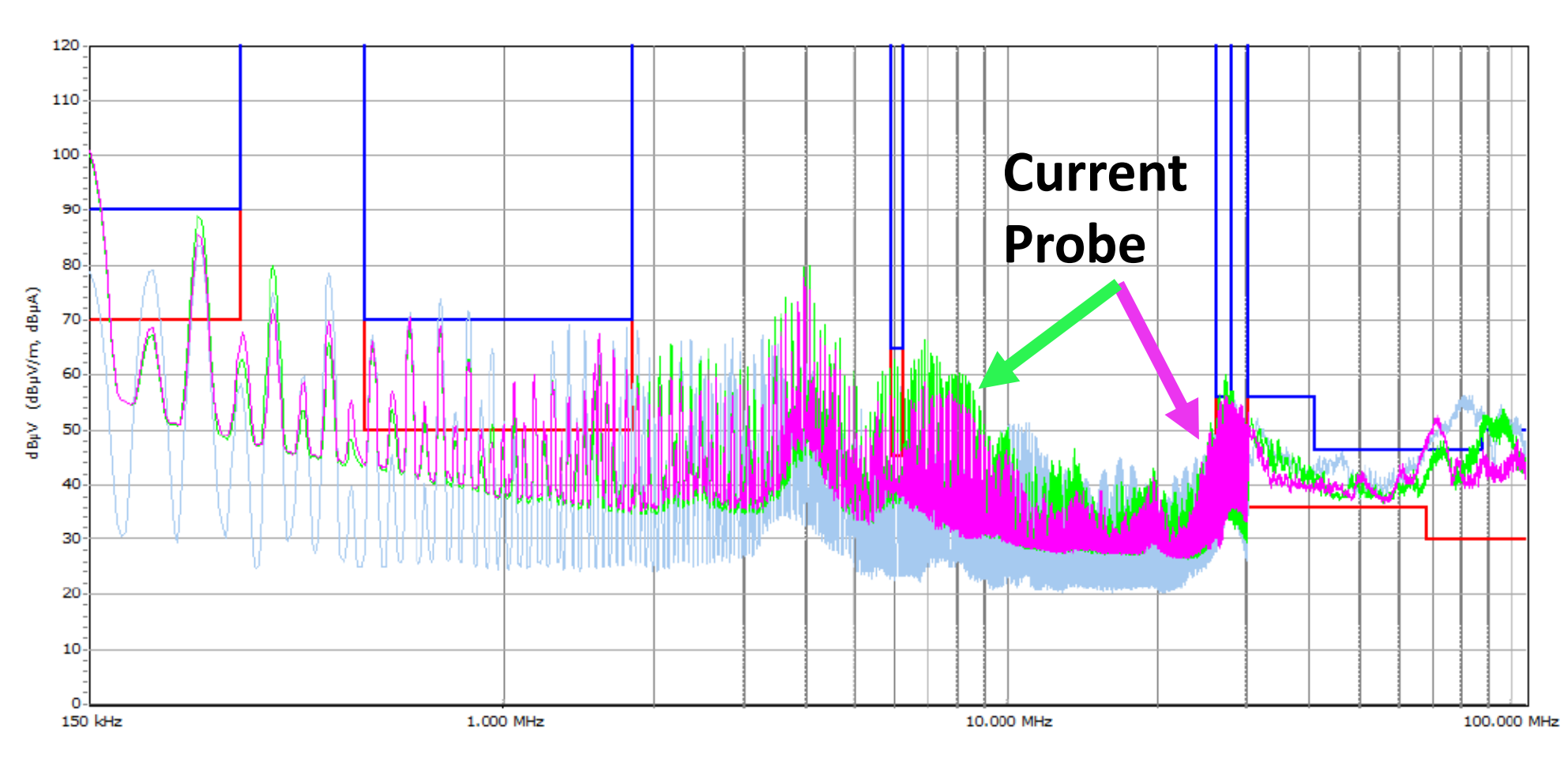
K. Y. See, "Network for conducted EMI diagnosis," IEE Electron. Lett., vol. 35, no. 17, pp. 1446–1447, Aug. 1999.

Current Probe & LISN Measurement

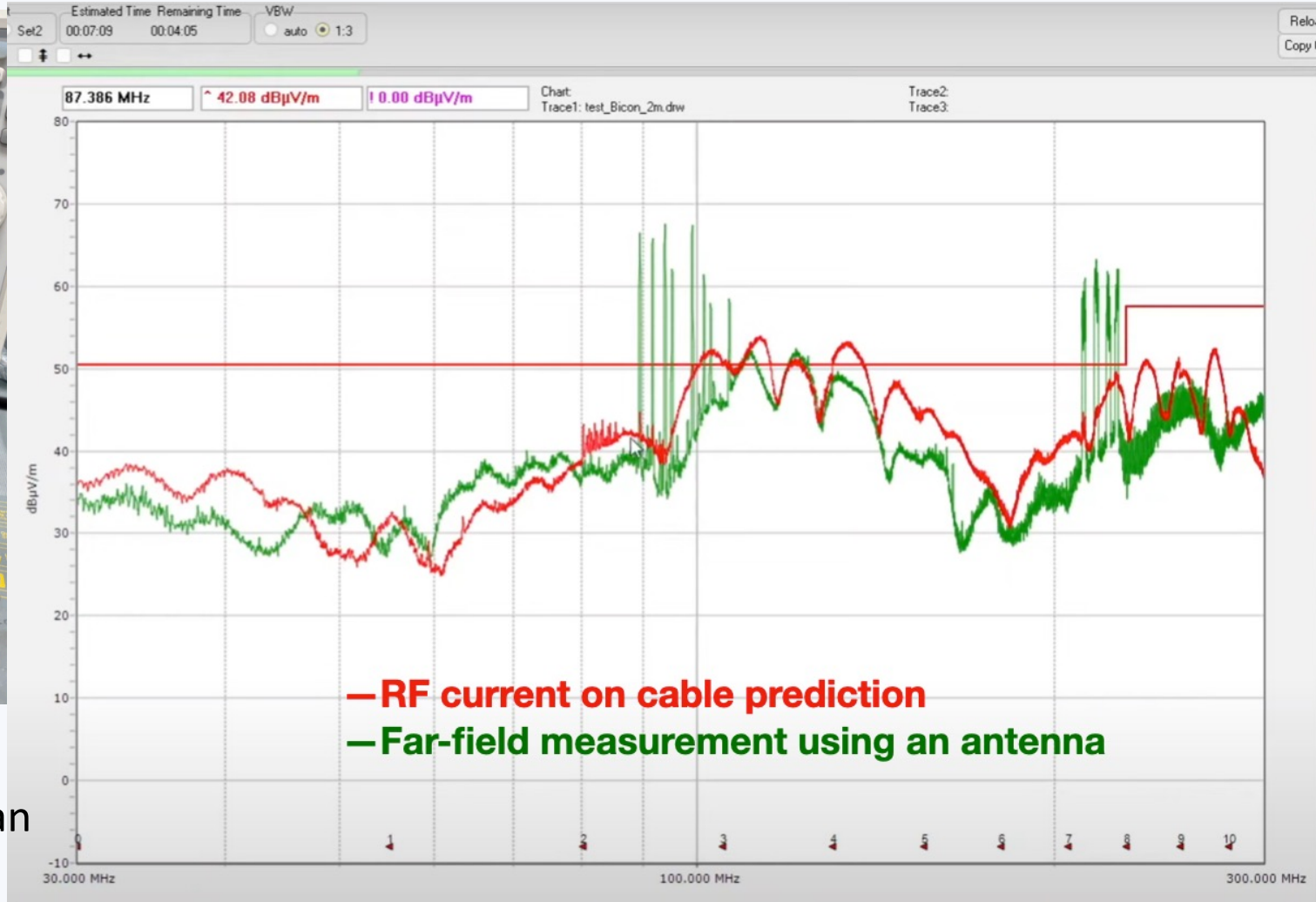
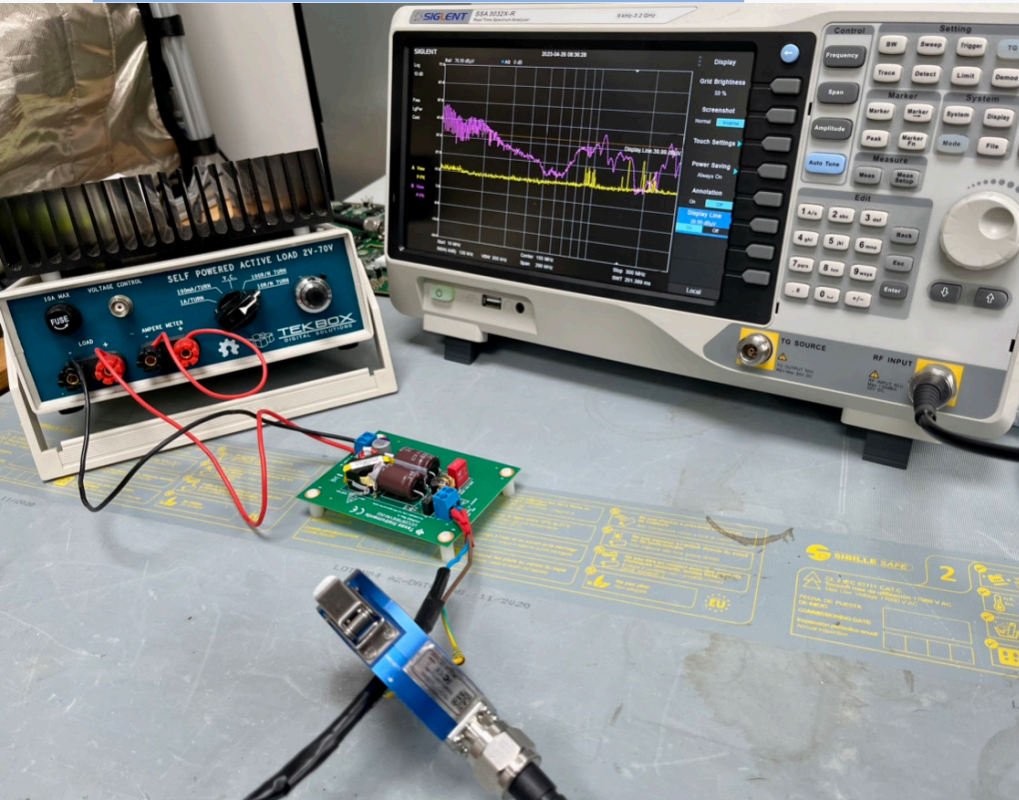
- Current probe method and the voltage method yield very similar results in lower frequencies, below 5 MHz.
- Difference in results in higher frequencies, above 5MHz.



Current Probe vs LISN Measurement

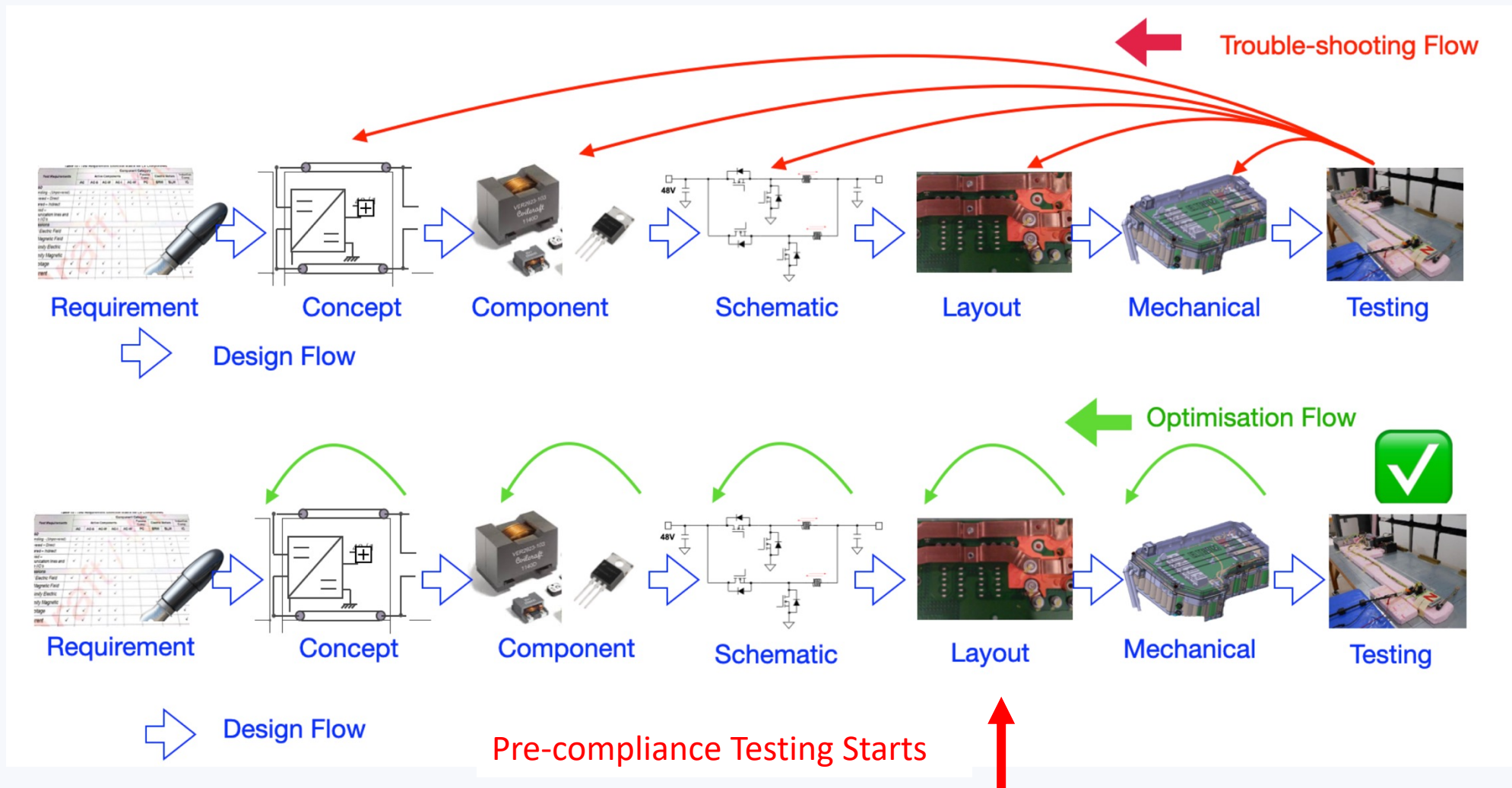


Using Current Probe Results to Predict Far-field Emissions

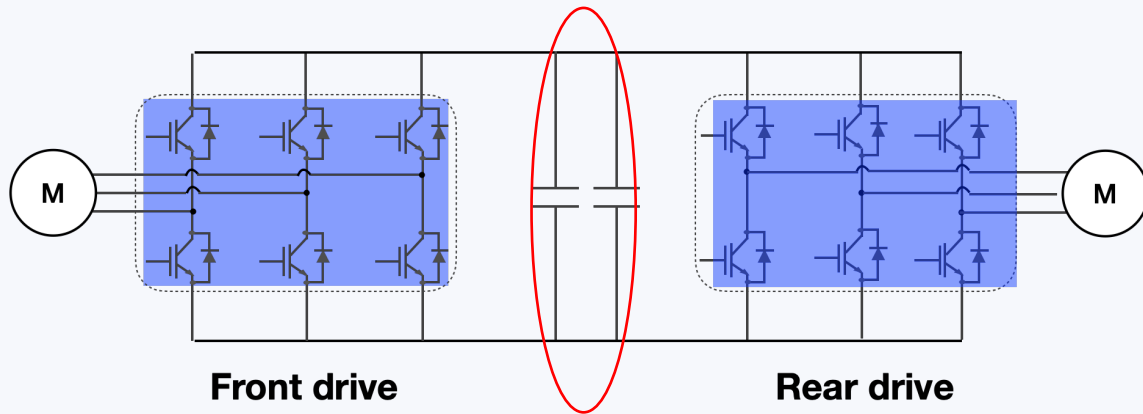


- Using an RF current probe to measure common mode current, far-field emission can therefore be predicted to a good accuracy

Design Strategies – EMC Planning & Management



Design Strategies – DC Link Design



- Does my DC Link has the least impedance (i.e., the smallest loop that I could achieve)?



The DC link was on the top side board, and the switches were on the bottom.

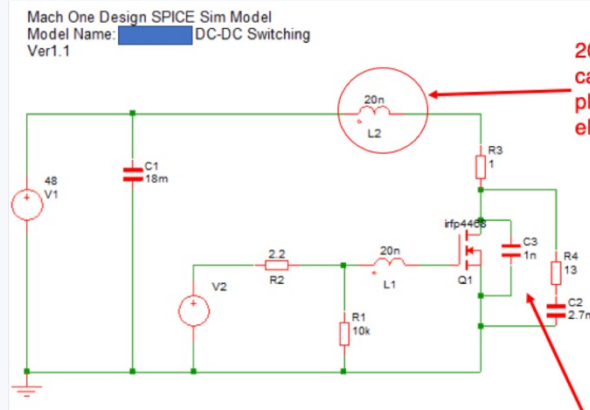
Design Strategies – Switching

Estimated 10 nH inductance introduced by the lead of the package.

IRFP4468PbF	
HEXFET® Power MOSFET	
V_{DSS}	100V
$R_{DS(on)}$ typ.	2.0m Ω
$R_{DS(on)}$ max.	2.6m Ω
I_D (Silicon Limited)	290A
I_D (Package Limited)	195A

TO-247AC

Source: Infineon (International Rectifier)

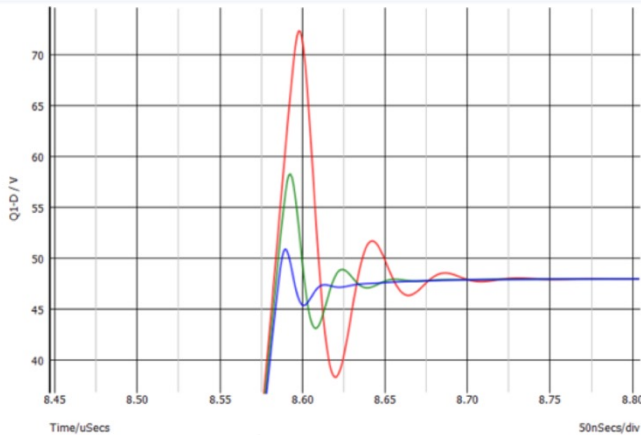


20 nH loop inductance, including 10 nH caused by the long lead of the device plus 10 nH of PCB tracks to the electrolytic capacitor

1nF parasitic capacitor of the device based on its packaging and layout

Comments: We often prefer SPICE based simulation as it is quick to build, can run very fast and leads to good understanding of the circuit behavior. This is extremely useful for troubleshooting as can be seen later.

- Through hole or SMD? - That is a question
- Soft switching or hard?
- Snubber?
- ZVS control?
- Spread spectrum or not?
- Covering the switch node with shielded inductor if applicable



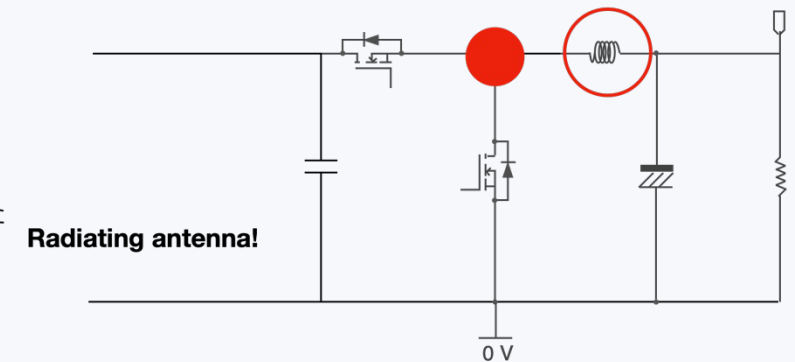
Loop inductance L2

— 20 nH
— 10 nH
— 5 nH

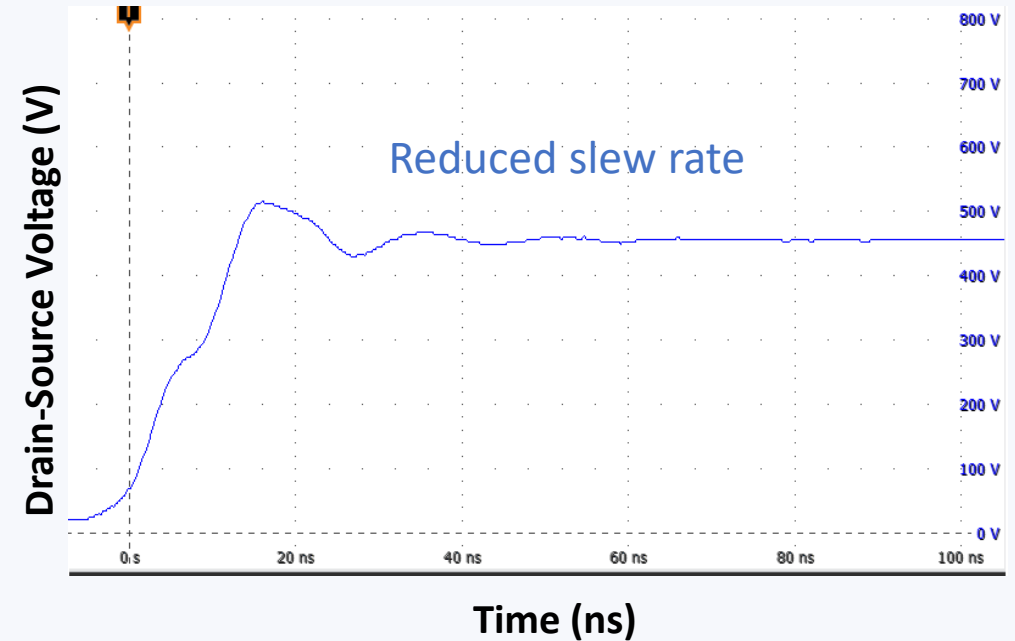
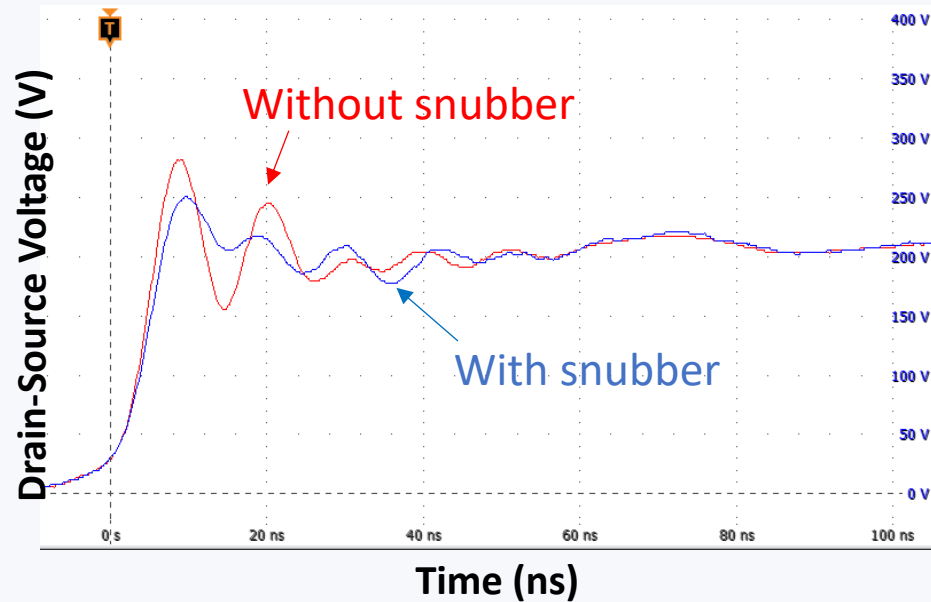
Unshielded - Not suitable



Use shielded inductor to shield the Switch Node

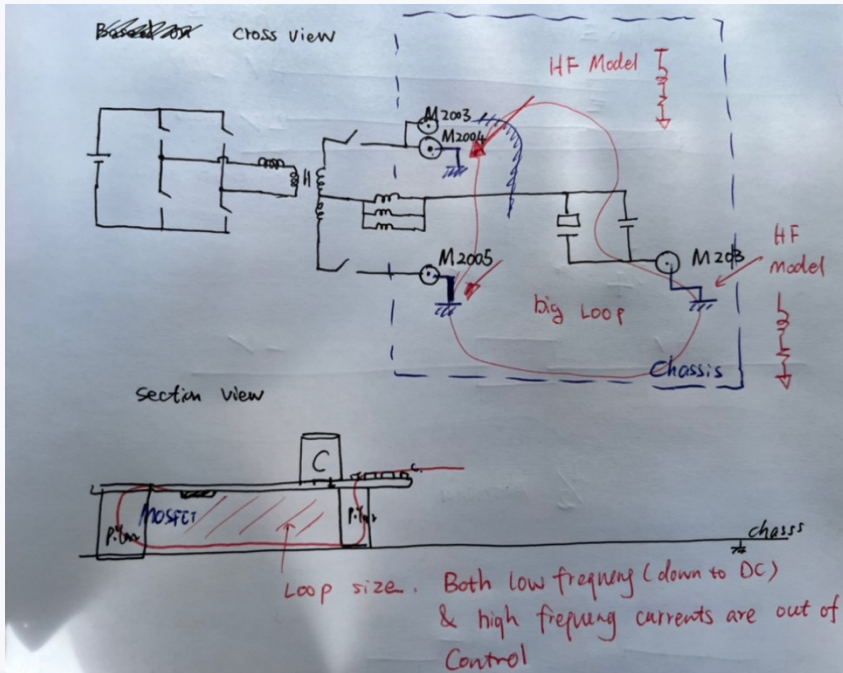
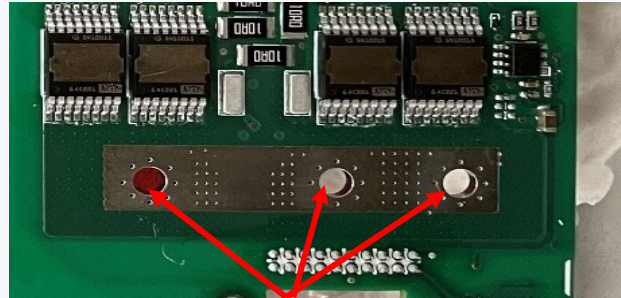
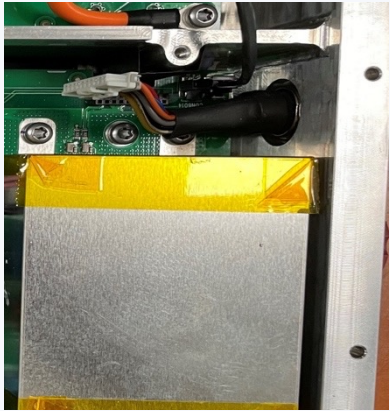


Switching Frequency and Speed

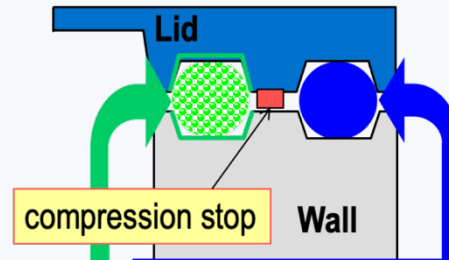
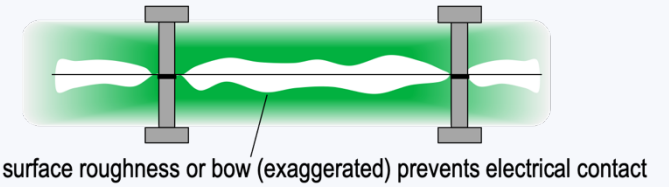


- Snubber damps the resonance of parasitic components
- Reduced ringing impacts EMI at the ringing frequency
- Spike killer noise suppression device (very lossy).
- Reduced slew rates impact EMI roll-off in the 30- to 200MHz band → effects efficiency

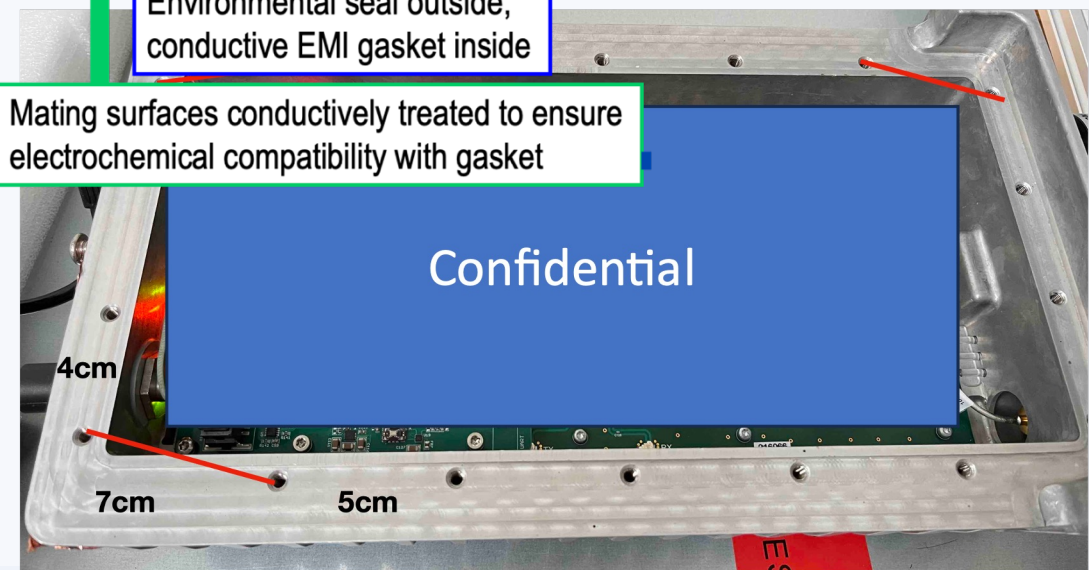
Design Strategies – Grounding and Shielding



A seam is just another aperture



Mating surfaces conductively treated to ensure electrochemical compatibility with gasket



Design Strategies – Active Filtering

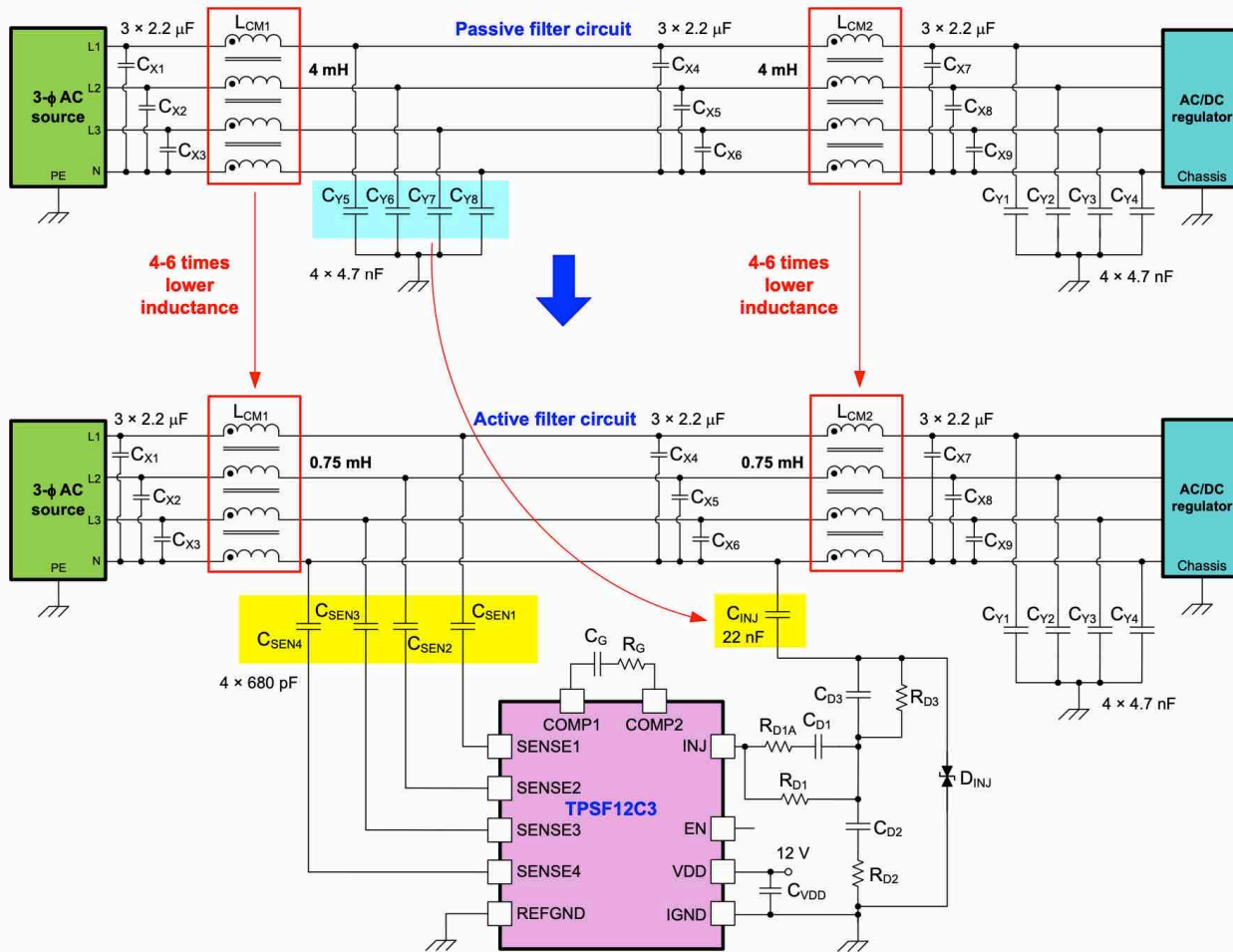
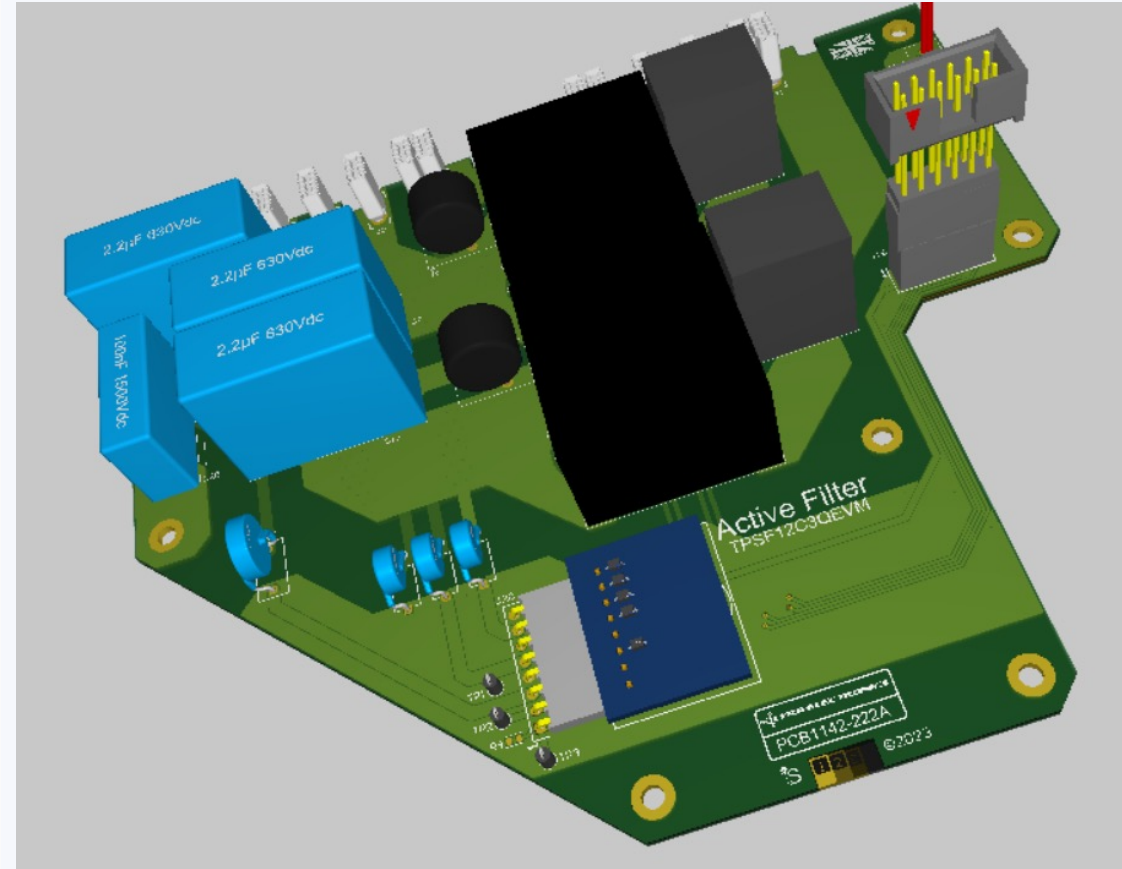


Figure 1-1. Three-Phase, Four-Wire Passive and Active Filter Schematics

Source: Texas instruments,



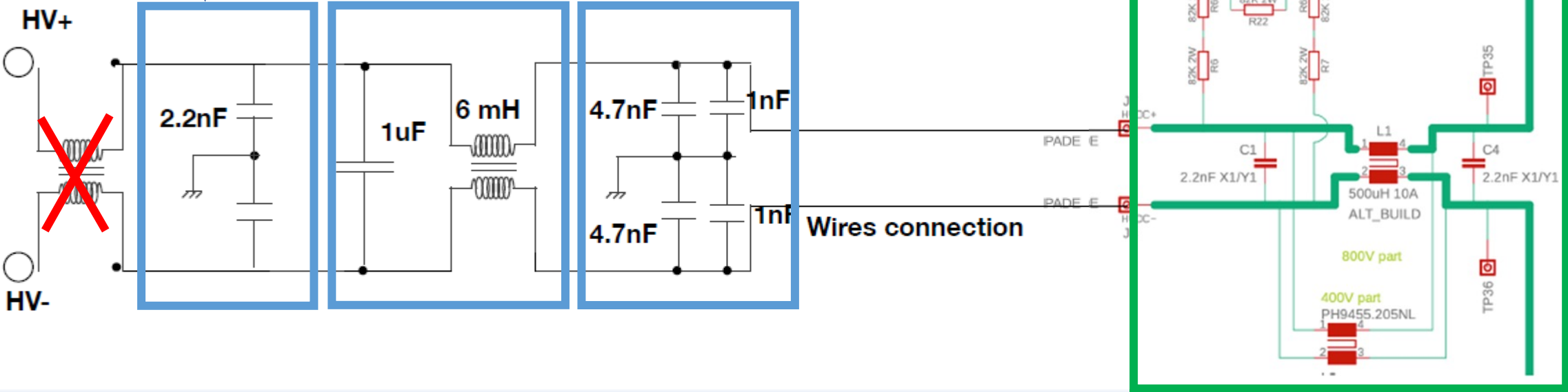
Case Study: EMI Reduction on the HV Line

Since unshielded cables were used on the HV line, the focus was to design a multi-stage front end filter

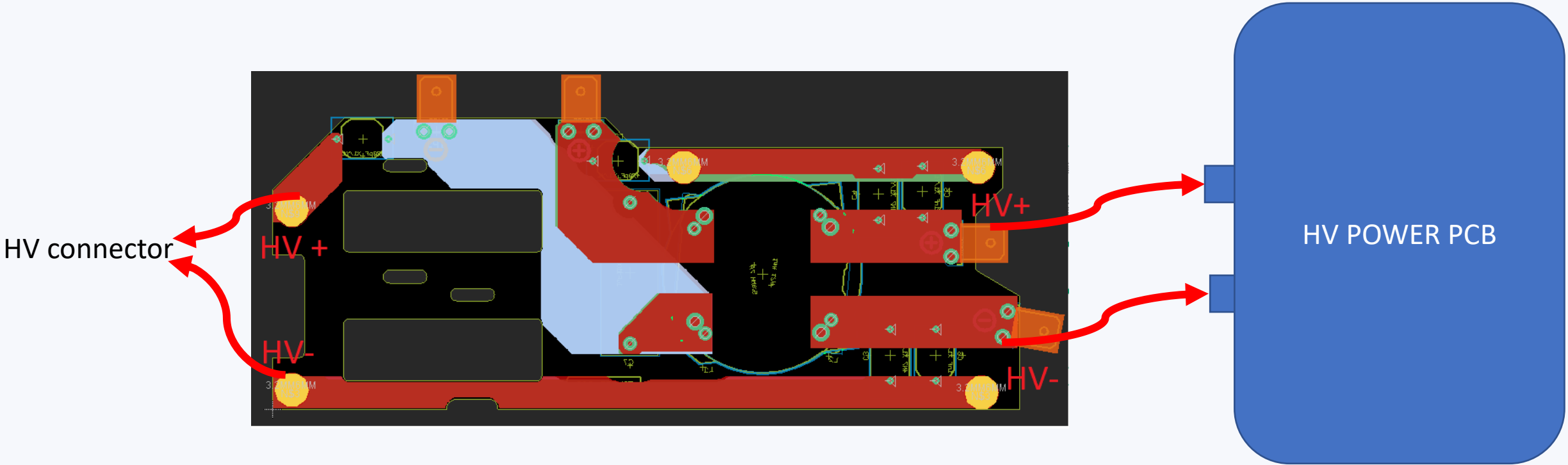
Improves emissions in the FM band

Improves low frequency performance

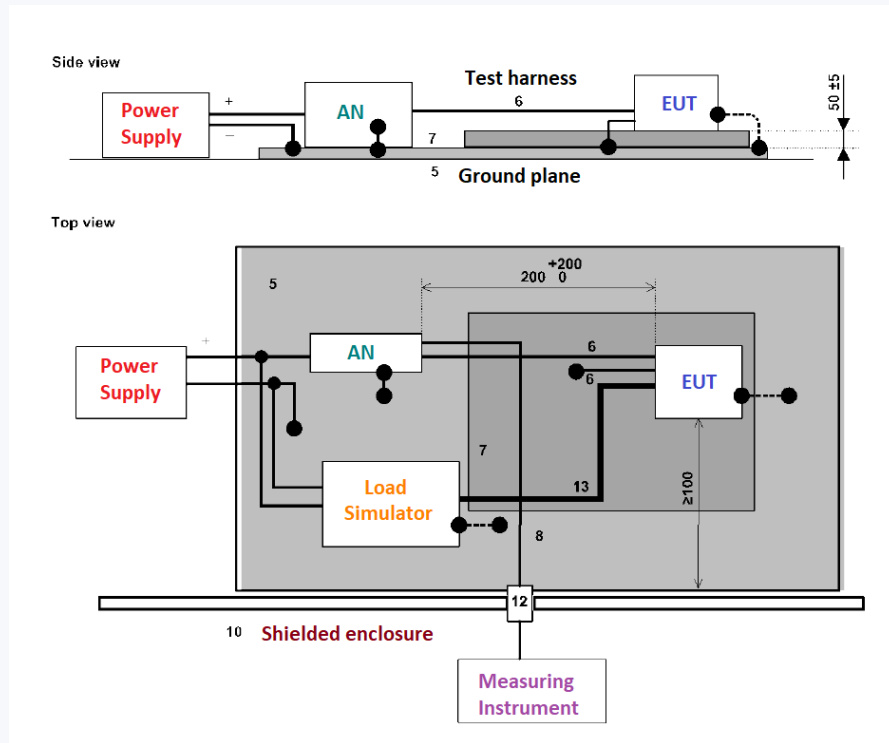
Improves high frequency performance



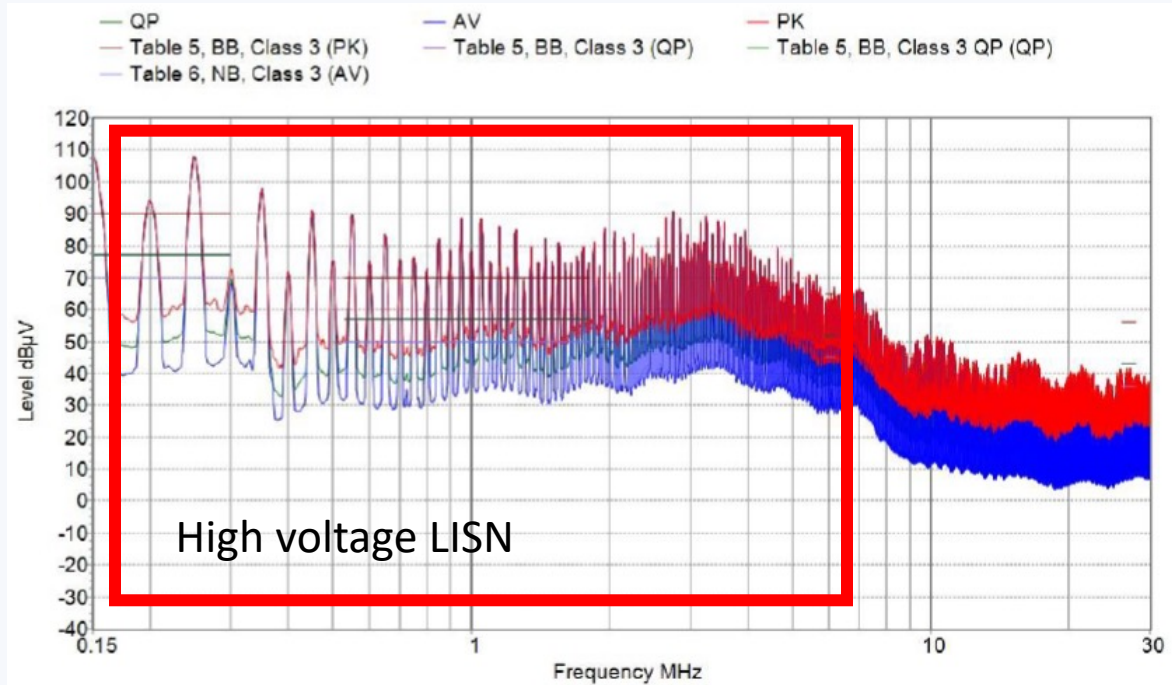
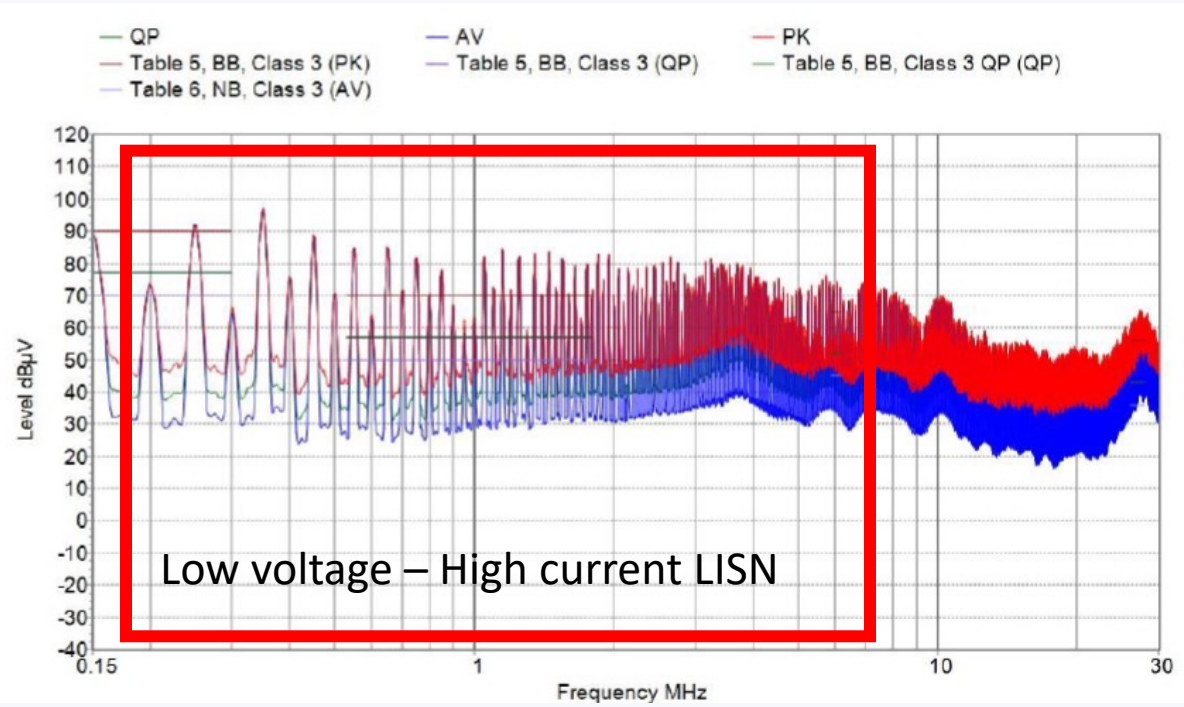
Design a Multi-stage Filter PCB



Chamber EMC Testing: Conducted Emissions

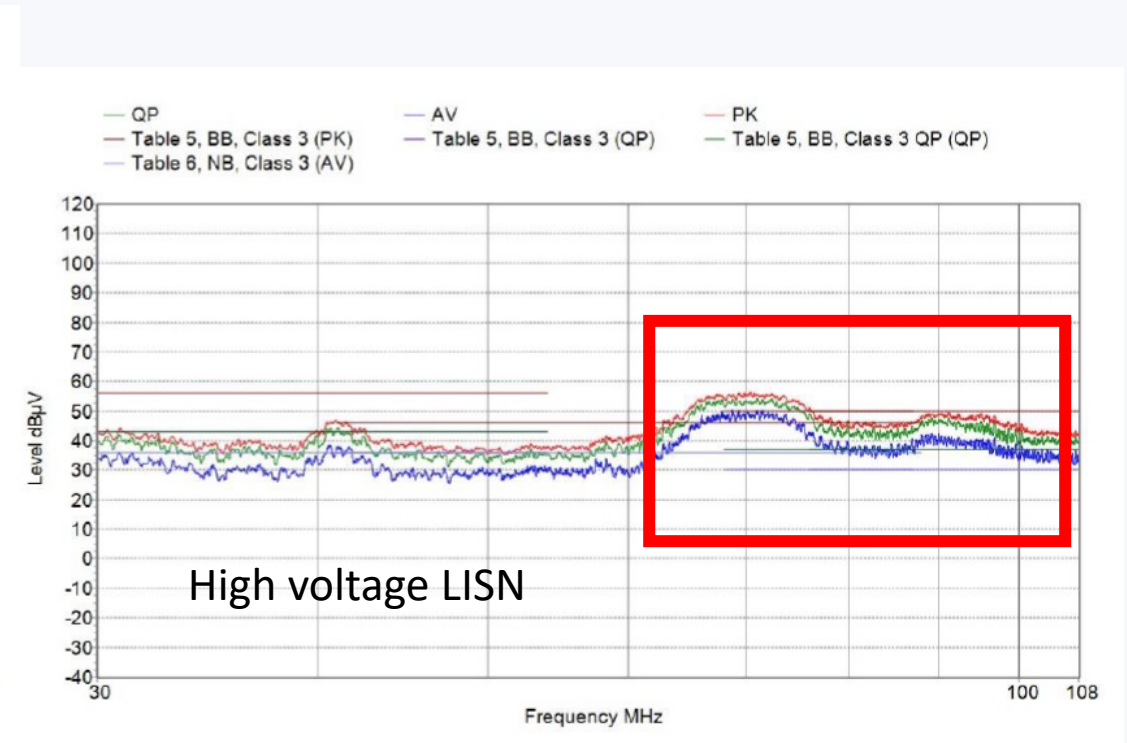
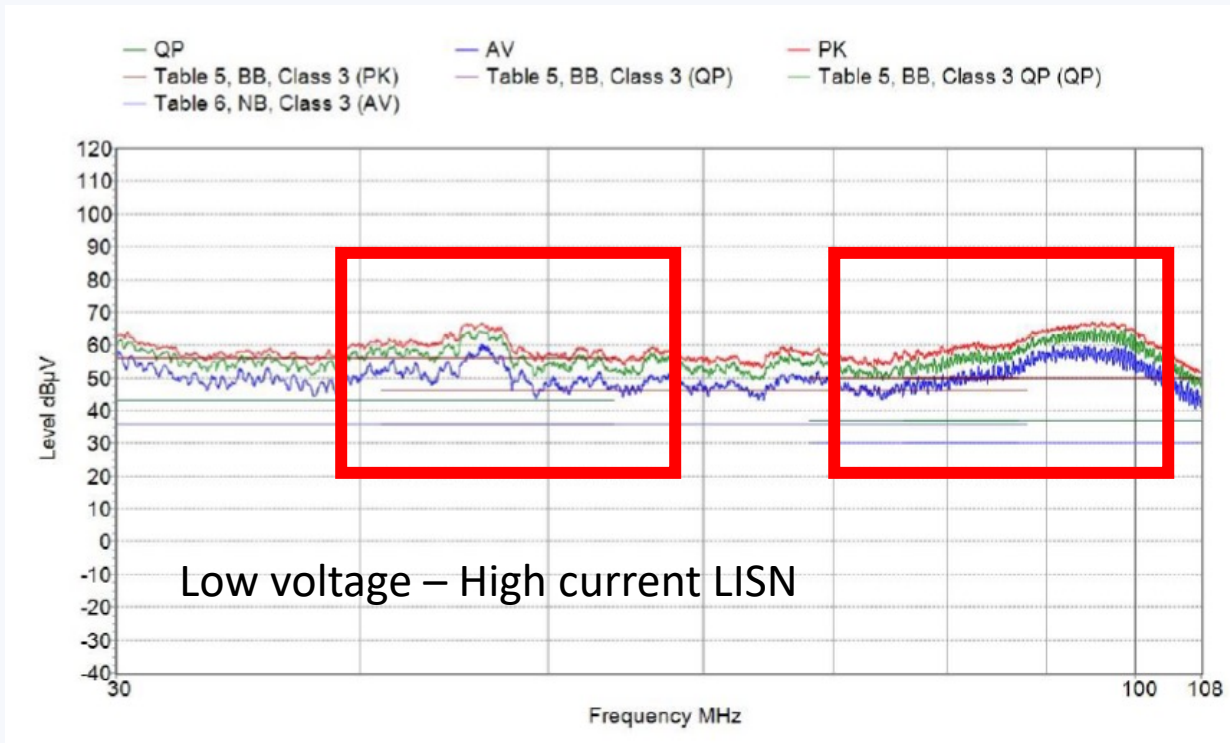


Conducted emissions analysis: the HV Line



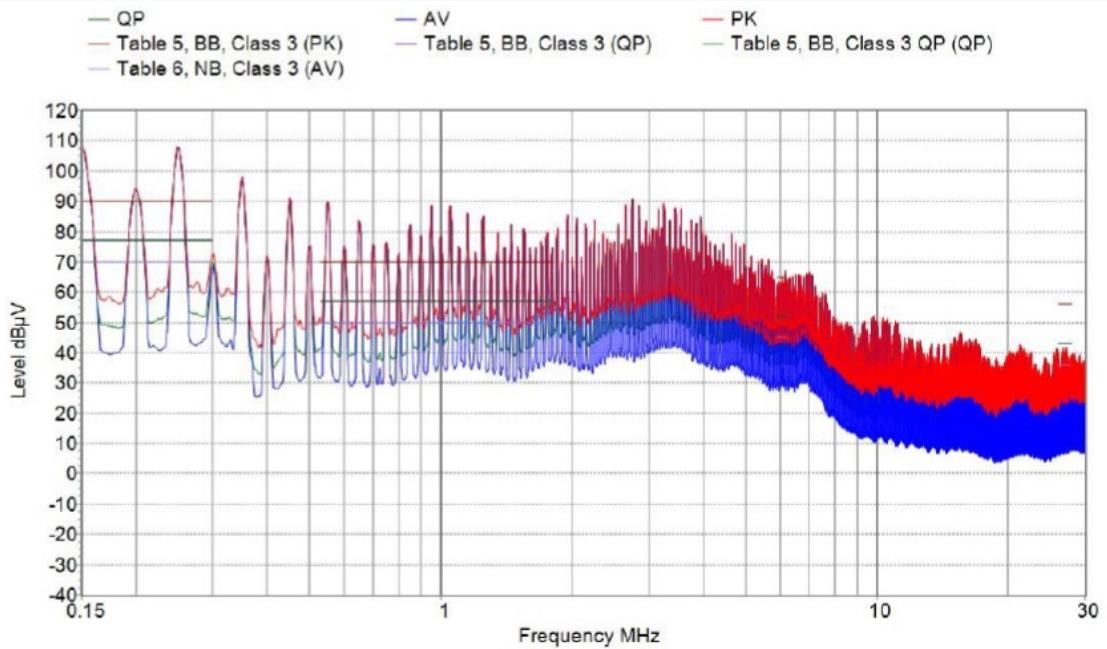
Switching frequency of the converter (50kHz) and its harmonics are the main frequency contents in the low frequency band

Conducted emissions analysis: the HV Line

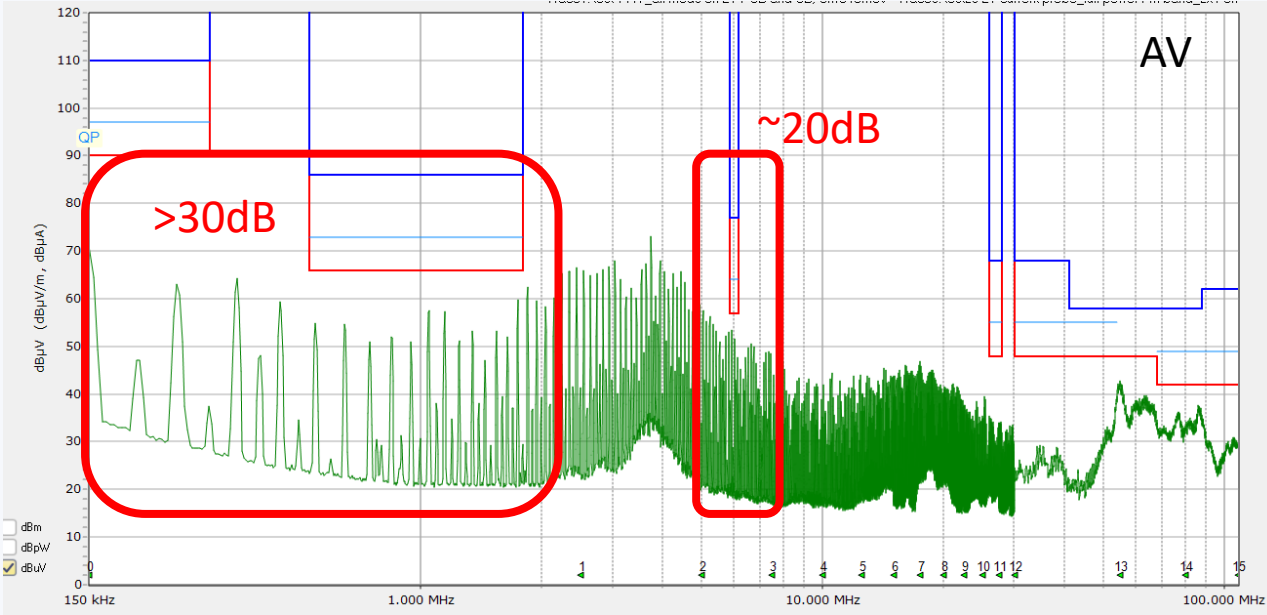


The conducted noise in this region will cause radiated emissions issue as the cables act as antennas.

Improved Result: the HV Line



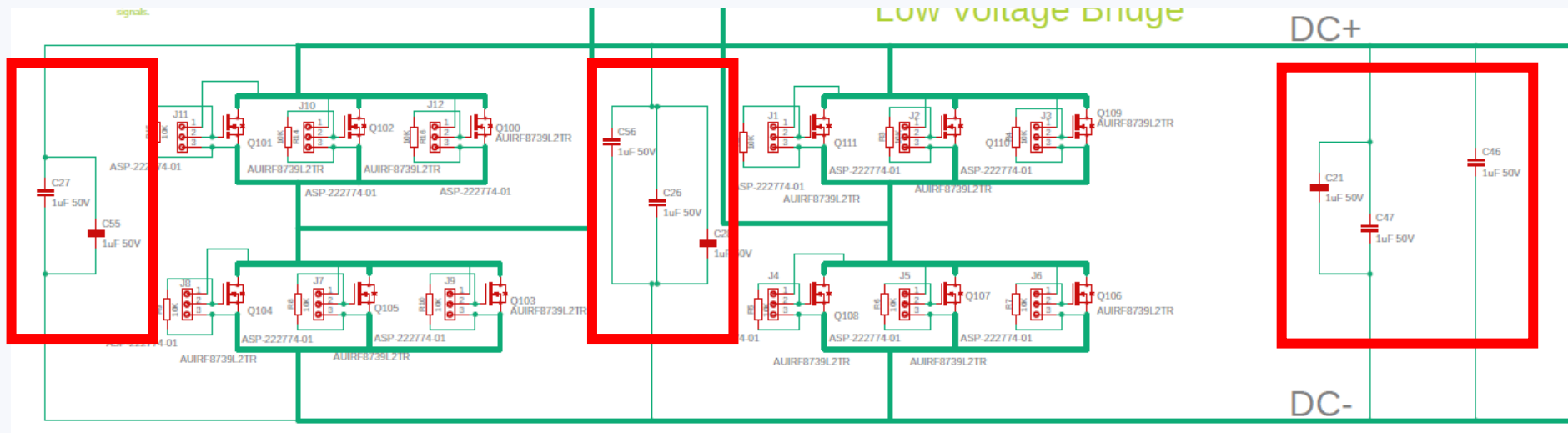
Without HV filter



With HV filter

EMI Reductions on the LV Line

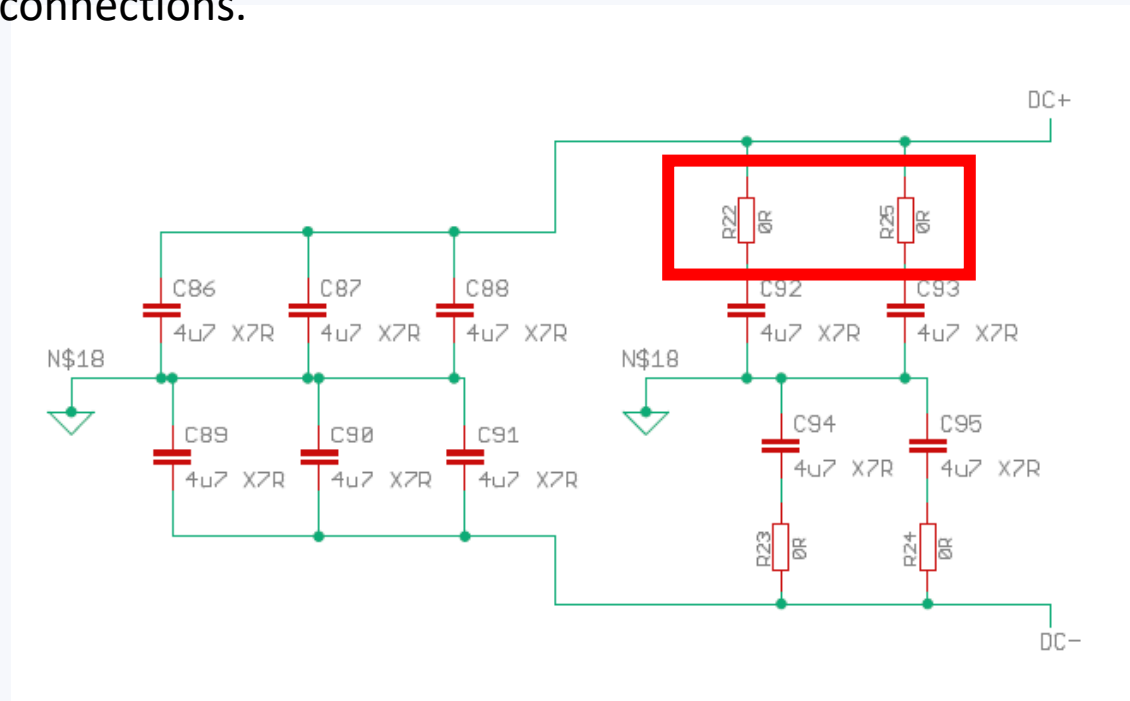
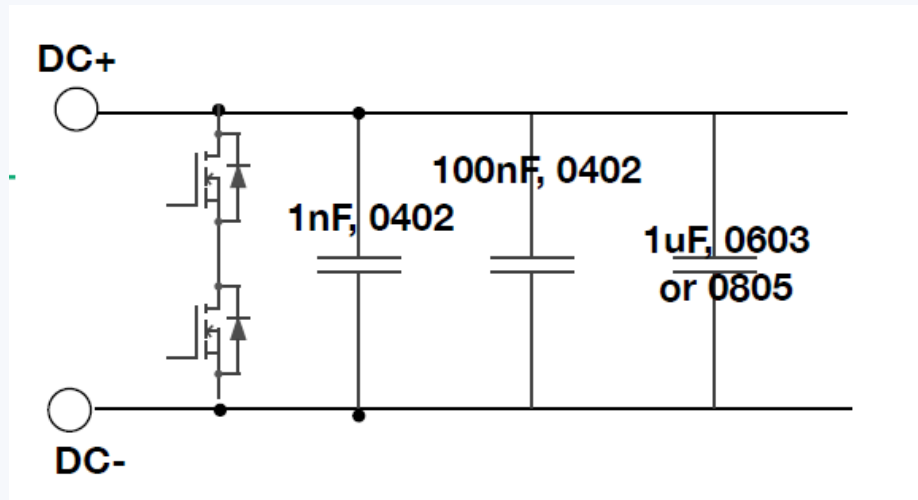
- Due to very high current on the LV line, we could only apply capacitors between the LV rails and the vehicle chassis.
- The key is to limit the impedance caused by the connections.
- Parallel MOSFETs



- 3x 1μF capacitors for each half bridge

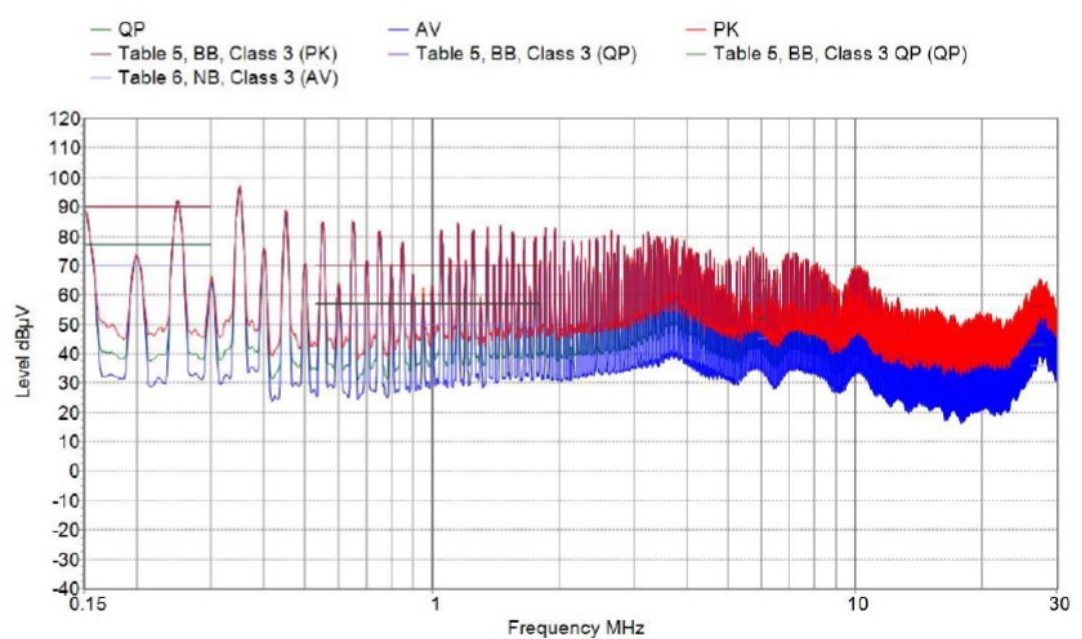
EMI Reductions on the LV Line

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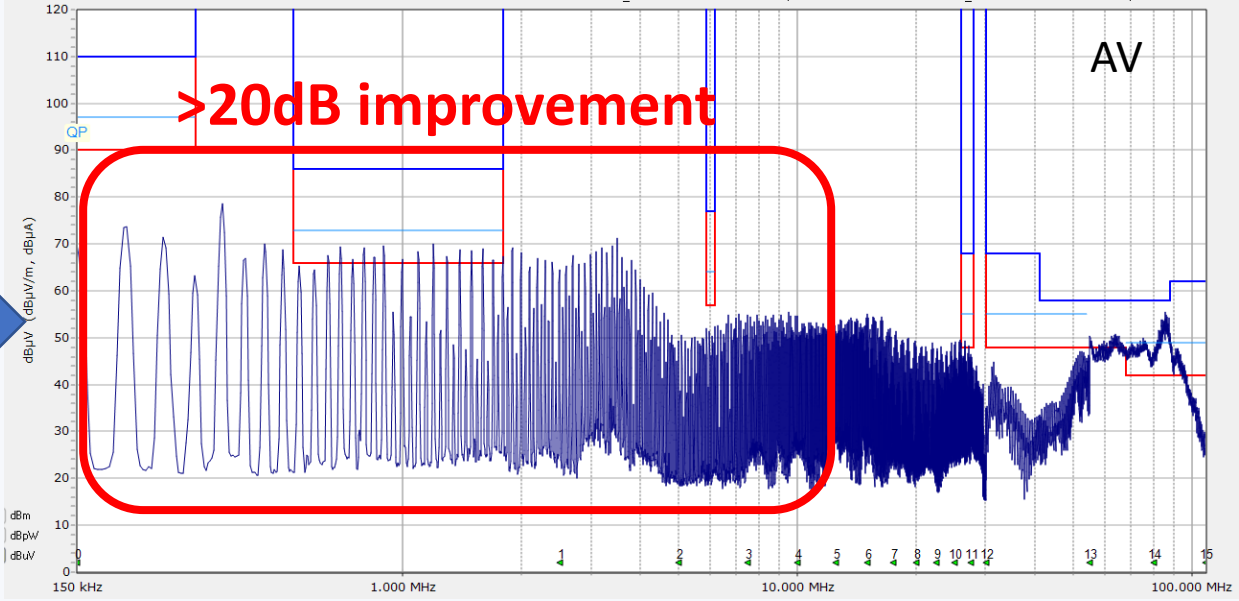


- Use low ESL and ESR capacitors
- MLCC capacitor bank → Cover wide frequency band
- Avoid resonance → Damping
- Parasitic components increase with package size

Improved Result: LV Line/High current



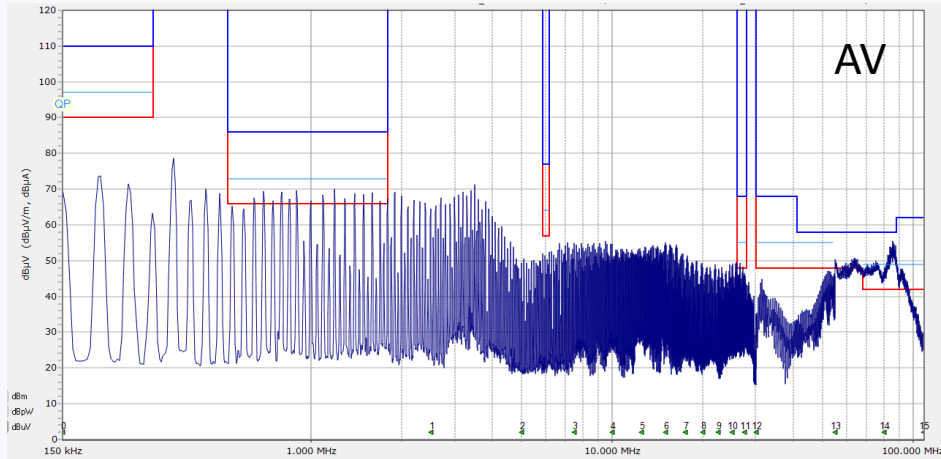
Before



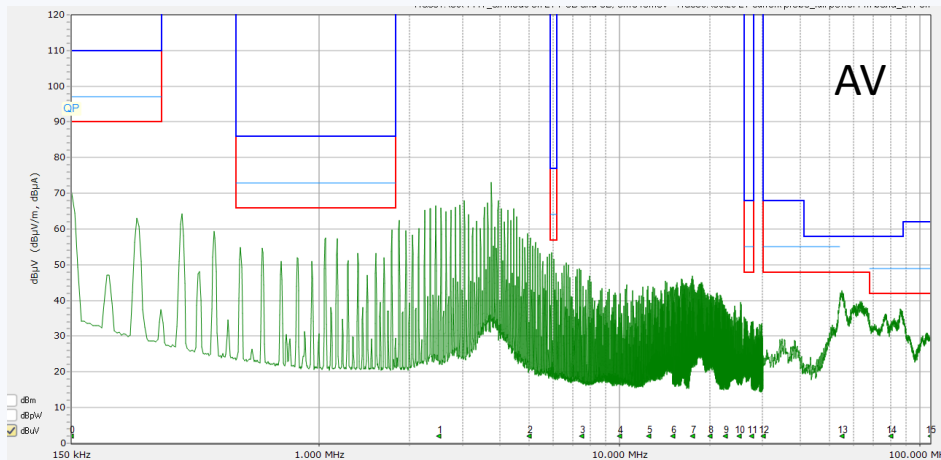
After

Software Switching Techniques: HV & LV Lines

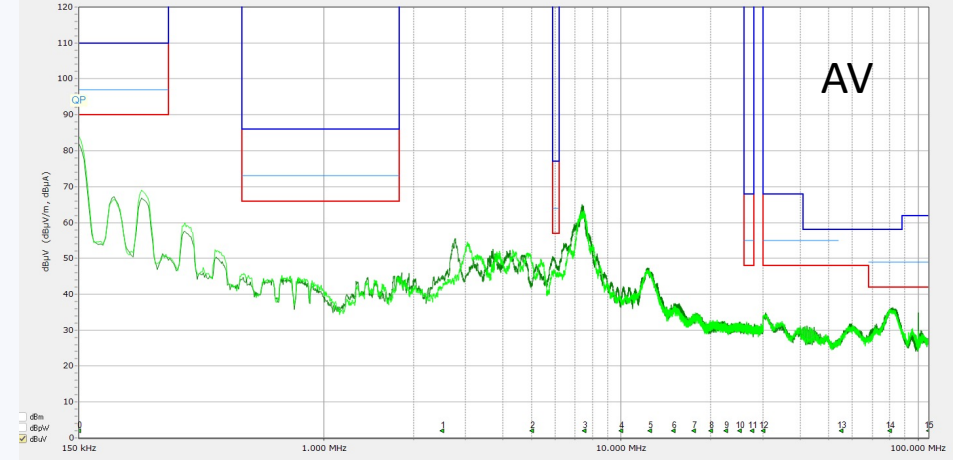
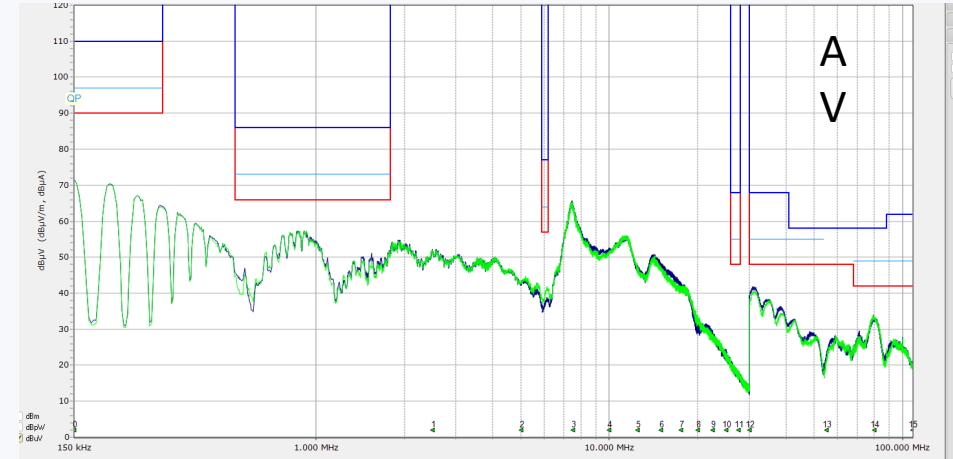
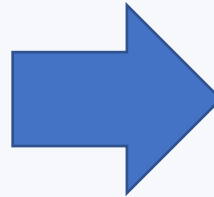
LV



HV



Before

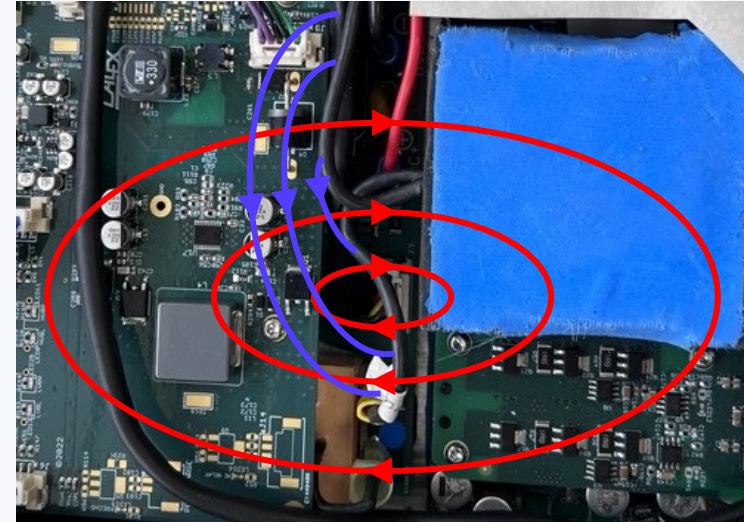


After

PCB design considerations

1. PCB design

- Select components and circuits with EMI in mind
- Design and enforce the ground system at the product definition stage
- Identify and label high di/dt circuits
- Component placement
- Careful PCB layout
- Minimise surface areas of nodes with high dv/dt



2. Cables

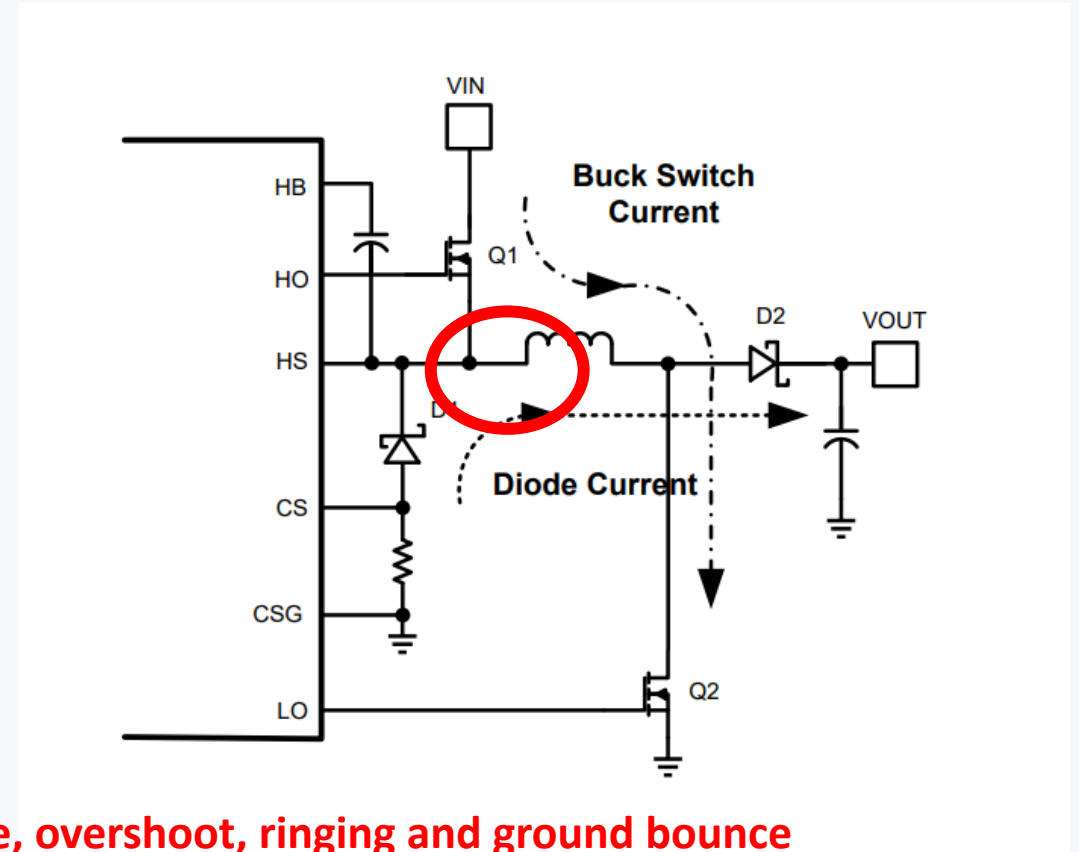
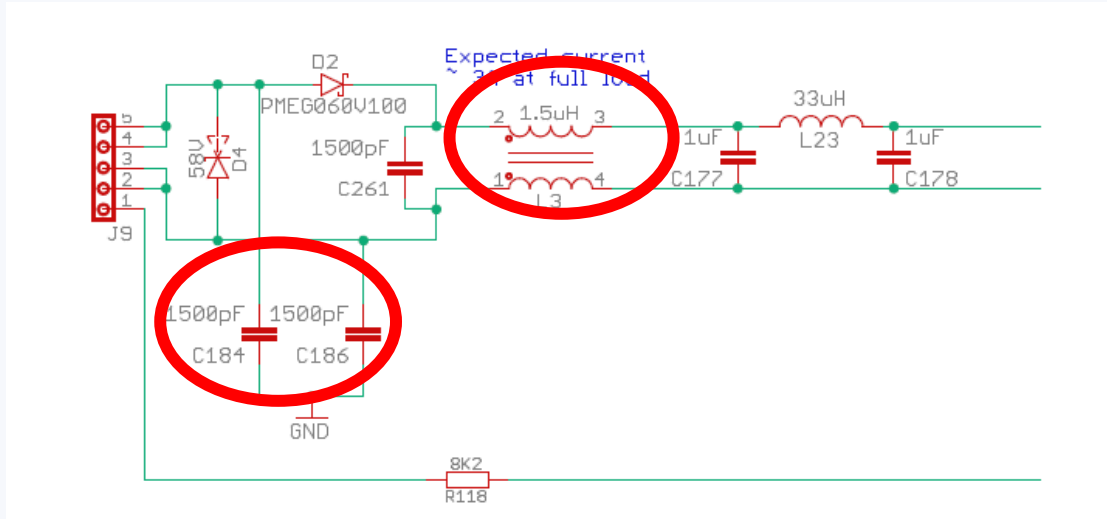
- Conducted path through cabling
- Cables can radiate



Pigtails here are a bad idea

3. Filters

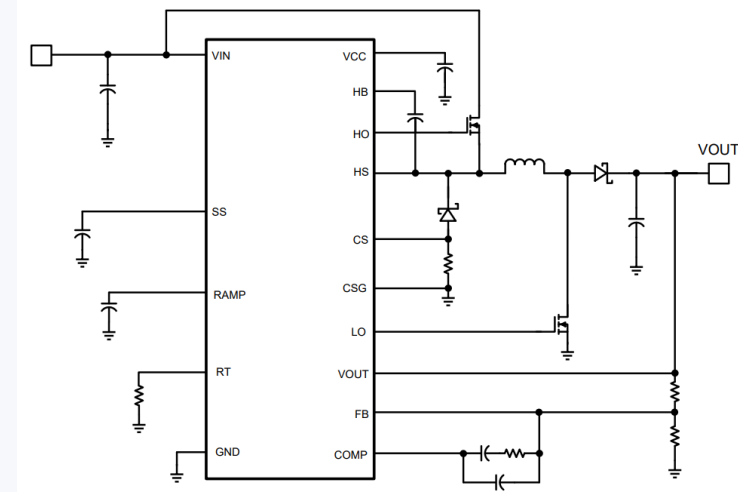
Identify Critical Loops with High di/dt Currents



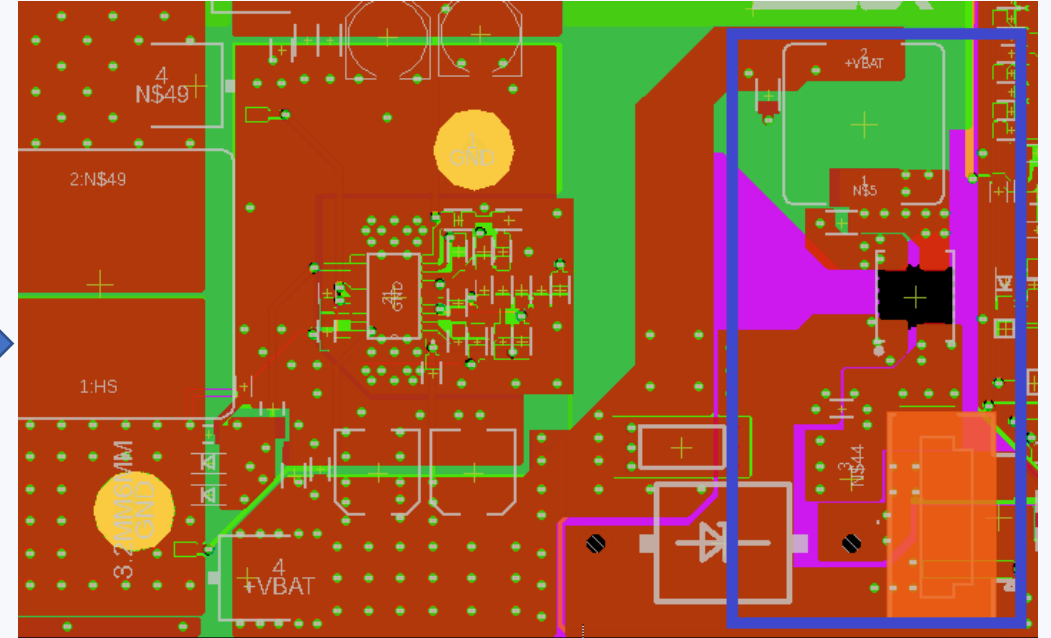
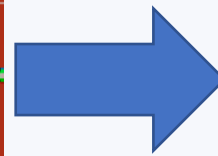
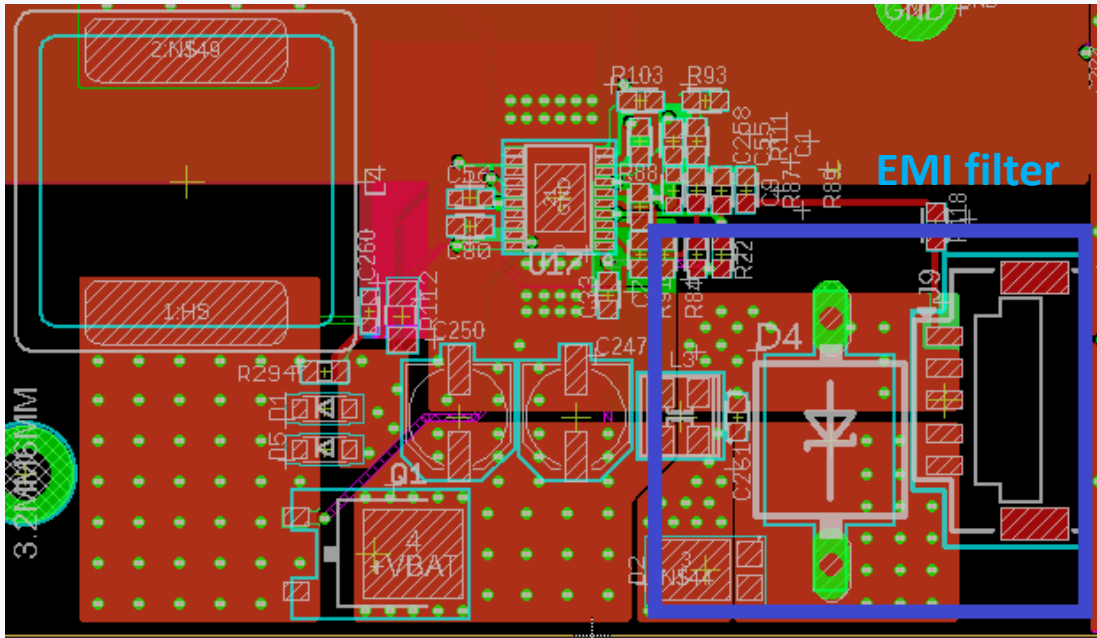
- Pinpoint high slew rate current (high di/dt) loops
- Identify layout-induced parasitic inductance that cause **noise, overshoot, ringing and ground bounce**
- “Shielded” inductor still emits significant EMI!
- Long connections from capacitors to chassis GND
- Improve buck-boost converter layout
- Replace common mode choke

High di/dt Loop

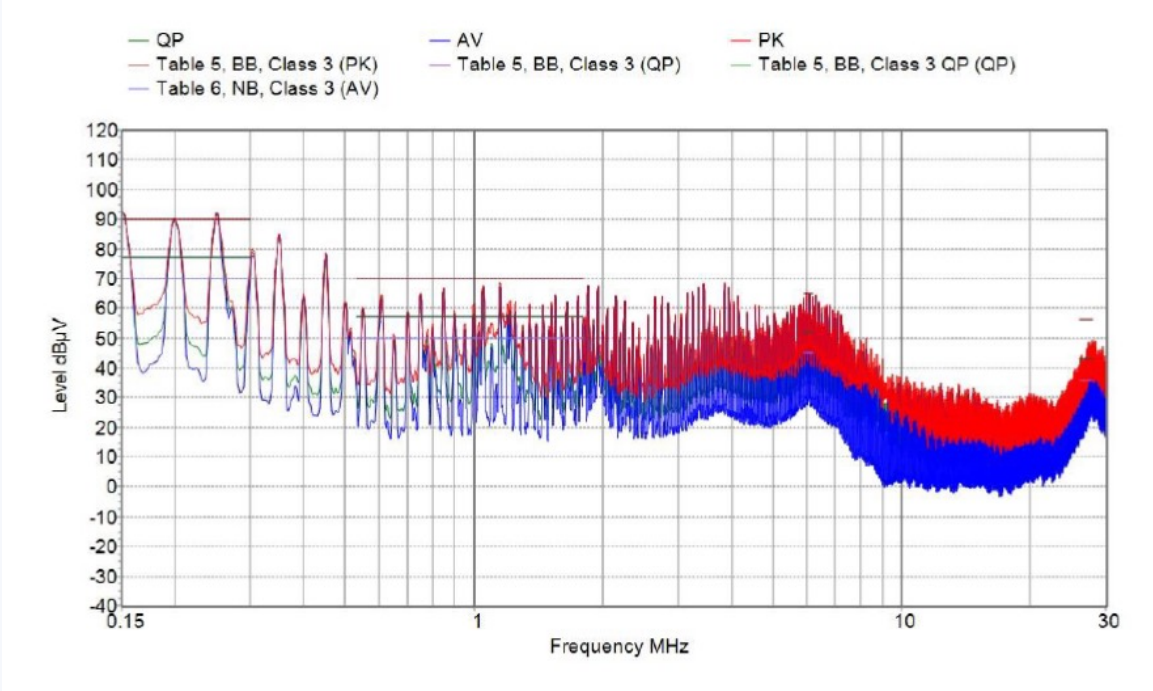
- Power stage shall be placed away from connectors and cables
- Power stage shall be placed away from filters
- Low ESR and ESL input and output capacitors
- EMI filter shall be close to the connector
- Ground plane shall not be broken



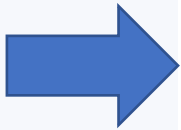
EMI filter



Improved Result: Low Voltage/Low Current Line

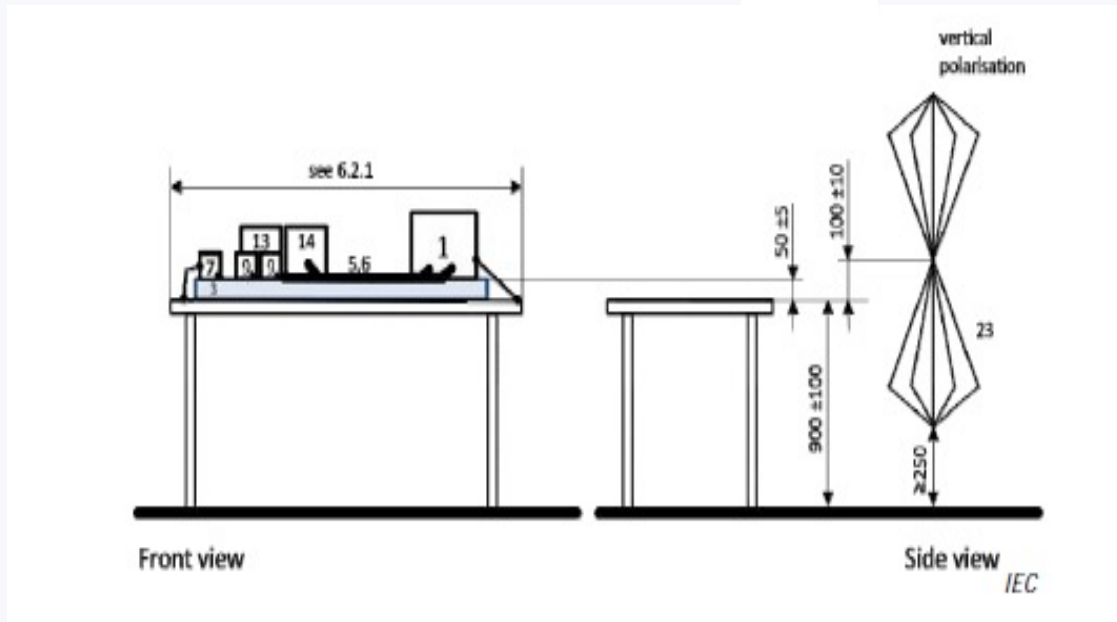


Before

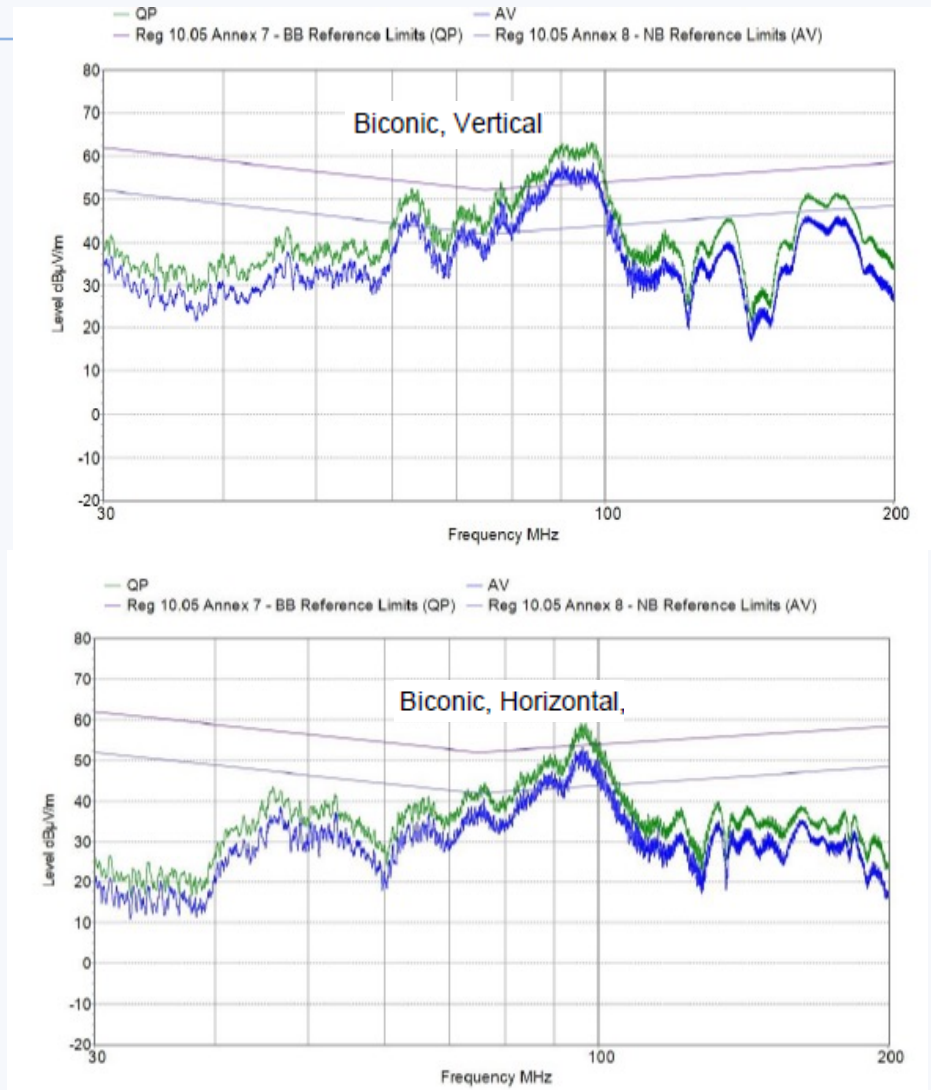


After

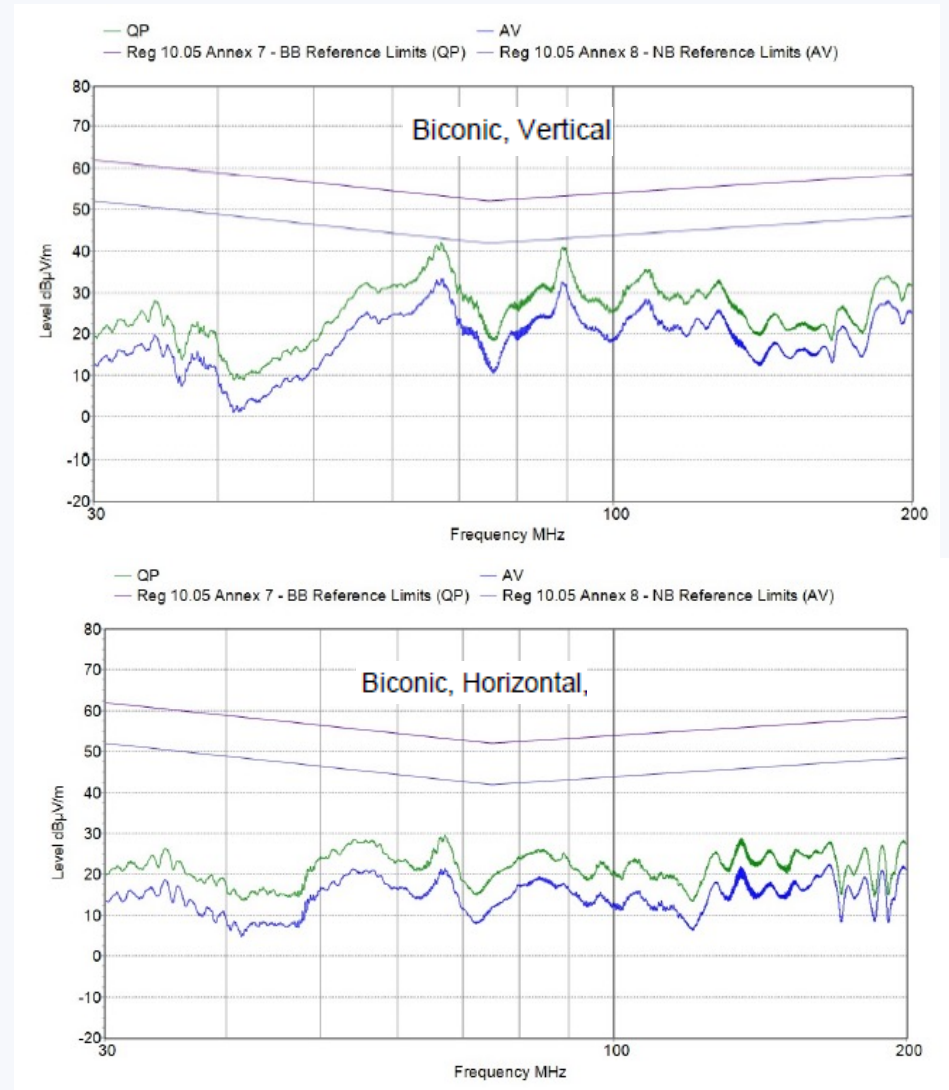
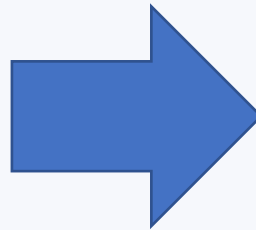
Chamber EMC Testing: Radiated Emissions



Radiated Emissions Test Results



BEFORE



AFTER



Thank you!

Any questions?

The logo for EMC & COMPLIANCE INTERNATIONAL features a green rectangular background at the top. Below this, a diagonal line divides the space into three colored sections: a red triangle on the left, a white triangle in the middle, and a blue triangle on the right. The text "EMC & COMPLIANCE INTERNATIONAL" is written in yellow, bold, uppercase letters across the green background.

**EMC &
COMPLIANCE
INTERNATIONAL**

<https://www.emcandci.com>

A promotional poster for EMC & CI 2024. The background is dark blue with a faint grid pattern. The text is in yellow and white. It includes the event name, a discount offer, dates, location, website, and email. There are two logos on the right side: the EMC & COMPLIANCE INTERNATIONAL logo and the MACHone logo.

EMC & CI 2024

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